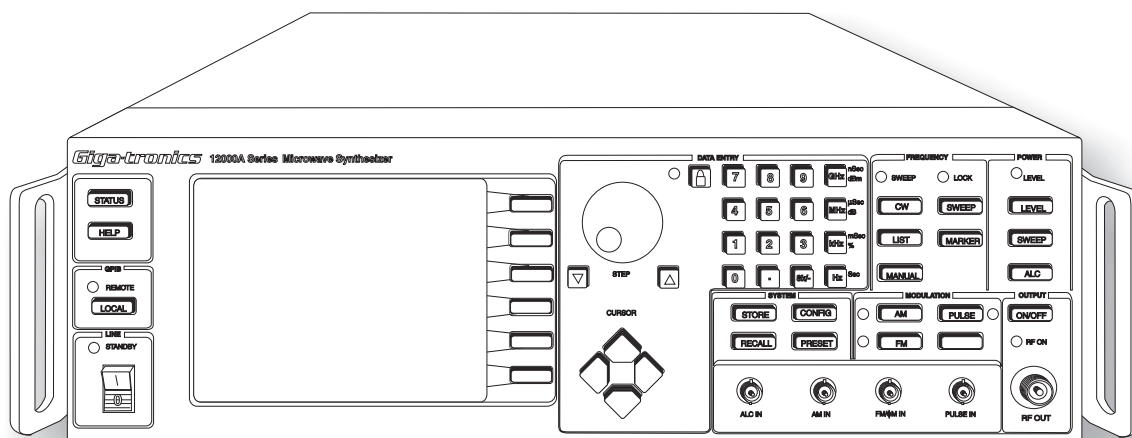




Series 12000A Microwave Synthesizers

Service Manual

12000A

CECertified Product
 ISO 9001Certified Process

Registrar: BSI, Certification No. FM 34226
 Registered 04 June 1996
 Amended on 01 March 2000

Giga-tronics Incorporated

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WARRANTY

Giga-tronics Series 12000A instruments are warranted against defective materials and workmanship for three years from date of shipment. Giga-tronics will at its option repair or replace products that are proven defective during the warranty period. This warranty DOES NOT cover damage resulting from improper use, nor workmanship other than Giga-tronics service. There is no implied warranty of fitness for a particular purpose, nor is Giga-tronics liable for any consequential damages. Specification and price change privileges are reserved by Giga-tronics.

Model Numbers

The series 12000A has model numbers for each instrument with a specific frequency range as described in Chapter 1. All models are referred to in this manual by the general term 12000A, except where it is necessary to make a distinction between the models. In these cases, the specific model number(s) will be used.

DECLARATION OF CONFORMITY

Application of Council Directive(s)

Standard(s) to which Conformity is Declared:

89/336/EEC and 73/23/EEC	EMC Directive and Low Voltage Directive
IEC 1010-1:1990 + A1: 1992	Safety
Modified: 1995 + A2	
EN61326-1 (1997)	EMC

Manufacturer's Name:

Giga-tronics Incorporated

Manufacturer's Address:

4650 Norris Canyon Road
San Ramon, California 94583
U.S.A.

Type of Equipment:

Microwave Synthesizer

Model Series Number:

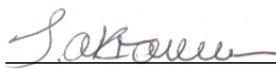
12000A

Model Number(s) in Series:

12508A, 12520A, 12522A, 12528A
12708A, 12720A, 12722A, and 12728A

I, the undersigned, hereby declare that the equipment specified above conforms to the above Directive(s) and Standard(s).

Thomas A. Kramer
(Full Name)


(Signature)

Director of Quality Assurance
(Position)

San Ramon, California
(Place)

July 28, 2000
(Date)

Preparation for Reshipment

Follow these instructions if it is necessary to return the product to the factory.

To protect the instrument during reshipment, use the best packaging materials available. If possible use the original shipping container. If this is not possible, a strong carton or a wooden box should be used. Wrap the instrument in heavy paper or plastic before placing it in the shipping container. Completely fill the areas on all sides of the instrument with packaging material. Take extra precautions to protect the front and rear panels.

Seal the package with strong tape or metal bands. Mark the outside of the package **“FRAGILE — DELICATE INSTRUMENT”**. If corresponding with the factory or local Giga-tronics sales office regarding reshipment, please reference the full model number and serial number. If the instrument is being reshipped for repair, enclose all available pertinent data regarding the problem that has been found.



NOTE: *If you are returning an instrument to Giga-tronics for service, first contact Giga-tronics Customer Service at **(800) 444-2878** or Telefax at **(925) 328-4702** so that a return authorization number can be assigned. You can also contact Customer Service via our e-mail address **repairs@gigatronics.com**.*

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About This Manual

This manual contains the following chapters to describe the service components of the Giga-tronics Series 12000A Microwave Synthesizers:

Preface:

In addition to a comprehensive Table of Contents and general information about the manual, the Preface also contains a record of changes made to the manual since its publication.

Chapter 1 - Specifications:

This chapter contains brief information about the instrument and provides information on its performance parameters.

Chapter 2 - Performance Tests:

This chapter defines the procedures to verify the performance of the Series 12000A Microwave Synthesizers.

Chapter 3 - Adjustments:

This chapter provides procedures for inspection, calibration and performance testing.

Chapter 4 - Theory of Operation:

This chapter provides an instrument block diagram level description and its circuits for maintenance and applications.

Chapter 5 - Replaceable Parts:

This chapter provides replaceable parts for the Series 12000A Microwave Synthesizers.

Chapter 6 - Troubleshooting:

This chapter contains procedures for troubleshooting.

Index:

A word index of the various elements of the Series 12000A Microwave Synthesizers Service manual.

Changes that occur after publication of the manual, will be inserted as loose pages in the manual binder. Please insert and/or replace the indicated pages as detailed in the Technical Publication Change Instructions included with new and replacement pages.

Conventions

The following conventions are used in this product service manual. Additional conventions not included here will be defined at the time of usage.

Warning

WARNING

The **WARNING** statement is encased in gray and centered in the page. This calls attention to a situation, or an operating or maintenance procedure, or practice, which if not strictly corrected or observed, could result in injury or death of personnel. An example is the proximity of high voltage.

Caution

CAUTION

The **CAUTION** statement is enclosed with single lines and centered in the page. This calls attention to a situation, or an operating or maintenance procedure, or practice, which if not strictly corrected or observed, could result in temporary or permanent damage to the equipment, or loss of effectiveness.

Notes



NOTE: A *NOTE* Highlights or amplifies an essential operating or maintenance procedure, practice, condition or statement.

[illegible]

Specifications

1.1 Introduction

The 12000A is a microwave synthesizer with step, ramp and list sweep capability; it operates over a wide range of microwave frequencies and power levels, and in a variety of modulation modes. The 12000A can generate output signals over a frequency range of 10 MHz to 20 GHz; the frequency range is dependent on the specific model number (see below). The RF output can be fixed (CW), step, ramp or list sweep with external frequency, amplitude, or pulse modulation.

Operation from the instrument front panel is detailed in Chapter 2 of the Series 12000A Operation Manual. Instructions on how to operate the instrument from a remote host computer over the General Purpose Interface Bus are in Chapter 3 (Operation Manual).

The following are the 12000A model numbers with their respective frequency range:

Table 1-1: 12000A Model Numbers

CW, Step, and List Sweep	CW, Step, Ramp, and List Sweeps	Frequency Range
Model 12508A	Model 12708A	10 MHz to 8 GHz
Model 12528A	Model 12728A	2 GHz to 8 GHz
Model 12520A	Model 12720A	10 MHz to 20 GHz
Model 12522A	Model 12722A	2 GHz to 20 GHz

1.1.1 Environmental Standards

The 12000A is environmentally tested for compliance with MIL-PRF-28800F, Class 3.

1.2 Performance Specifications

CW Operation

Range:	0.01 to 8 GHz; 2 to 8 GHz; 0.01 to 20 GHz; and 2 to 20 GHz.
Resolution:	0.1 Hz (standard); 1 kHz (with Option 36).
Accuracy and Stability:	Identical to time base oscillator.
Time Base (Internal):	10 MHz.
Aging Rate:	$<1 \times 10^{-9}$ /day after 72 hours continuous operation ($<5 \times 10^{-10}$ /day with Option 28).
Temperature Stability:	$<\pm 2 \times 10^{-10}$ /°C (0 to +55 °C).
Time Base (External):	5 or 10 MHz, $\pm 1 \times 10^{-6}$ or better; 0.5 to 5 V _{P-P} into 500 Ω , nominal.
Switching Time:	$<500 \mu\text{s}$ to within 1 kHz of set frequency with Residual FM (0.3 - 3 kHz) of 3 kHz RMS for 1 ms.

RF Output

Maximum Leveled Output
(0 to 35 °C):

Frequency Range	Standard	Option 26
.01 to 2.0 GHz	+15 dBm	+14 dBm
>2.0 to <8.0 GHz	+15 dBm	+15 dBm
8.0 to 15.0 GHz	+15 dBm	+13 dBm
>15.0 to 20.0 GHz	+15 dBm	+12 dBm

Incremental Level Range:	-20 to +20 dBm.
Resolution:	0.01 dB, entry and display.
Minimum Calibrated Output Level:	-10 dBm (-120 dBm with Option 26).
RF Off:	Attenuates the output to ≤ -140 dBm at the output connector.
Output Flatness:	(Internally leveled, CW frequency sweep mode or ramp mode) 15 to 35 °C $\leq \pm 0.5$ dB (0 dBm to maximum specified power). Add ± 0.1 dB/10 dB with Option 26.
Output Accuracy:	± 0.7 dB.
Maximum Slope of Level Variation:	<0.5 dB/MHz.
Output Switching Time:	$<500 \mu\text{s}$; 20 ms with attenuator change (Option 26).
Output Impedance:	50 Ω , nominal.
Output SWR:	$<2.0:1$.
External Leveling:	Output power may be externally leveled by positive or negative ZBS detectors or power meters.
Level Drift:	<0.05 dB/hour, maximum: 0.1 dB/24 hours.

Spectral Purity

Harmonics:

Frequency (GHz)	Harmonic (dBc)	Power (dBm)
.01 to 0.1	-30	+6
>0.1 to 2.0	-50	+6
>2.0 to 20	-60	+6

Subharmonics: -65 dBc.

Nonharmonics: <-60 dBc (0.01 to 16 GHz); <-55 dBc (>16 to 20 GHz).

Single-Sideband Phase Noise: dBc/Hz, CW mode, all power levels:

Freq (GHz)	Offset from Carrier				
	100 Hz	1 kHz	10 kHz	100 kHz	1 MHz
0.25	-96	-101	-109	-122	-124
0.5	-90	-95	-103	-122	-124
2.0	-78	-92	-94	-120	-125
4.0	-73	-86	-88	-110	-130
6.0	-73	-84	-85	-110	-130
8.0	-67	-80	-82	-105	-130
10.0	-67	-80	-82	-105	-125
18.0	-61	-75	-75	-100	-120
20.0	-61	-75	-75	-100	-120

Residual FM: Hz, RMS, CW mode:

Frequency Range (GHz)	Post-detection Bandwidth	
	300 Hz to 3 kHz	50 Hz to 15 kHz
<2.0	Decreases by 1/2 per oct	Decreases by 1/2 per oct
2 to 3.99	<6	<35
4 to 7.99	<12	<70
8 to 15.99	<24	<140
16 to 20	<32	<200

AM Noise: ≤130 dB/Hz (0.01 to 2.0 GHz); ≤145 dBm/Hz (>2.0 GHz); Typical 5 MHz offset.

Ramp Frequency Sweep

Continuous sweep:	Generated within the instrument, can be operated simultaneously with Step power sweep.
Range:	From FA (minimum frequency of instrument) to FB (maximum frequency of instrument).
Sweep Time:	1 ms to 200 s (any sweep mode).
Resolution:	10 μ s.
Minimum Sweep Time:	Determined by the sweep width and the maximum sweep speed.
Minimum Sweep Width:	100 Hz (1 MHz with Option 36).
Minimum Sweep Speed:	100 kHz/sec.
Maximum Sweep Speed:	1 Octave/8 ms (general spec) determined by the frequency band.
Band Crossing Dead Time:	<400 μ s.
Sweep Width Resolution:	0.1 Hz (1 kHz with Option 36).
Start, Stop, Halted Frequency Accuracy:	Phase-locked to time base.
Sweep Linearity:	<0.5% of sweep width (relative to the linear 0 to +10V Ramp Out voltage, sweep time $\geq$ 10 ms, any sweep mode).
Sweep Modulation Formats:	AM or Pulse Modulation.
Ramp Sweep Mode:	
Start/Stop:	$FA \leq [F1 \neq F2] < FB$ Sweeps up or down from a preset start frequency (F1) to a preset stop frequency (F2).
Start/ Δ :	$FA \leq [F1 \pm \Delta F] \leq FB$ Sweeps up or down from a preset start frequency (F1) through a preset sweep width (ΔF).
CTR/ Δ :	$FA \leq [CF \pm (\Delta F/2)] \leq FB$ Sweeps up or down through a preset sweep width (ΔF) centered symmetrically about a preset center frequency (CF).
Δ MKR:	$FA \leq [Mx \neq My] \leq FB$ Sweeps up or down from any preset marker (Mx) to any other preset marker (My).
Ramp Sweep Functions:	
Auto:	Continuous cycle of the preset sweep.
Single:	A single cycle of the preset sweep, initiated by manual operation of the front panel pushbutton or reception of the corresponding GPIB command.
EXT:	A single cycle of the preset sweep, initiated by a trigger input from an external source.
Manual:	Stops the sweep when activated by the front panel pushbutton, the assertion of the Stop Sweep I/O BNC, or the reception of the corresponding GPIB command to enable manual tuning of the frequency at any point in the sweep. Permits continuation of the current frequency.
Frequency Markers (Step and Ramp frequency sweep):	
Resolution:	Sweep width $\div$ 4000.
Accuracy:	Same as Sweep linearity except the marker may vary $\pm$ 25 mV relative to the linear 0 to +10 V Ramp Out.
Amplitude Markers:	A -10 to +10 dB change in RF output during Ramp frequency sweep.
Video Markers:	TTL-level output or $\pm$ 5 V.
Intensity Markers:	Provides a timed dwell of frequency sweep.

Step Frequency Sweep

Range:	FA (minimum frequency of instrument) to FB (maximum frequency of instrument).
Step Size:	Any increment within the frequency resolution.
Dwell Time:	May be set in 1 ms increments from approximately 1 ms to 200 sec.
Setup Time:	200 μ s/step, typical.
Accuracy And Stability:	Same as in CW when locked at each step during dwell time.
Step Sweep Modes:	
<i>Start/Stop:</i>	$FA \leq [F1 \neq F2] \leq FB$ Sweeps up or down from a preset start frequency (F1) to a preset stop frequency (F2).
<i>Start/Δ:</i>	$FA \leq [F1 \pm \Delta F] \leq FB$ Sweeps up or down from a preset start frequency (F1) through a preset sweep width (ΔF).
<i>CTR/Δ:</i>	$FA \leq [CF \pm (\Delta F/2)] \leq FB$ Sweeps up or down through a preset sweep width (ΔF) centered symmetrically about a preset center frequency (CF).
<i>Start/Steps:</i>	$FA \leq [F1 \pm (\text{step size} \times \text{no. of steps})] \leq FB$ Sweeps up or down from a preset start frequency (F1) through a preset number of frequency steps.
Step Sweep Functions:	
<i>Auto:</i>	Continuous cycle of the preset sweep.
<i>Single:</i>	A single cycle of the preset sweep or (with stop activated) a single preset step, initiated by the front panel pushbutton or reception of the corresponding GPIB command.
<i>EXT:</i>	A single cycle of the preset sweep initiated by each trigger from an external source.
<i>EXT Step:</i>	A single step of a preset step sweep, initiated by each trigger input from an external source.
<i>Manual:</i>	Stops the sweep when activated by the front panel pushbutton, assertion of the Stop Sweep I/O BNC, or reception of the corresponding GPIB command to enable manual tuning of the frequency to any point in the sweep. Permits continuation from the current frequency.

Ramp Power Sweep

Continuous sweep, generated within the instrument. Can be operated simultaneously with Ramp or Step frequency sweep.

Range:	-10 dBm to maximum power (-120 dBm to maximum power with Option 26).
Sweep Time (any sweep mode):	2 ms to 200 ms in five ranges. Minimum sweep time is determined by the sweep width and the maximum sweep speed.
<i>Minimum Sweep Width:</i>	0.01 dB.
<i>Maximum Sweep Speed:</i>	1 dB/ms.

Range	Resolution
2.0 to 20.0 ms	10.0 μ s
20.0 ms to 200.0 ms	100.0 μ s
200.0 ms to 2.0 sec	1.0 ms
2.0 sec to 20.0 sec	10.0 ms
20.0 sec to 200.0 sec	100.0 ms

Sweep Level Resolution (any sweep mode):	0.01 dB.
Start Level Accuracy (any sweep mode):	± 0.5 dB (-10 to +11 dBm).
Sweep Level Linearity (any sweep mode):	$\pm 5\%$ of sweep width.

Ramp Power Sweep Modes:

<i>Start/Stop:</i>	$LA \leq [L1 \neq L2] \leq LB$ Sweeps up or down from a preset start level (L1) to a preset stop level (L2).
<i>Start/Δ:</i>	$LA \leq [L1 \pm \Delta L] \leq LB$ Sweeps up or down from a preset start level (L1) through a preset sweep width (ΔL).
<i>Ctr/Δ:</i>	$LA \leq [CL \pm (\Delta L/2)] \leq LB$ Sweeps up or down through a preset sweep width (ΔL) centered symmetrically about a preset center level (CL).

Ramp Power Sweep Functions:

<i>Auto:</i>	Continuous cycle of preset sweep.
<i>Single:</i>	A single cycle of the preset sweep, initiated by manual operation of the front panel pushbutton or reception of the corresponding GPIB command.
<i>EXT:</i>	A single cycle of the preset sweep, initiated by a trigger input from an external source.
<i>Manual:</i>	Stops the sweep when activated by the front panel pushbutton, the assertion of the Stop Sweep I/O BNC, or the reception of the corresponding GPIB command to enable manual setting of the level to any point in the sweep. Permits continuation of the current level.

Step Power Sweep

Range:	LA (minimum level of instrument) to LB (maximum level of instrument).
Step Size:	Any multiple of 0.01 dB up to maximum sweep range.
Dwell Time:	May be set in 1 ms increments from approximately 1 ms to 200 sec.
Setup Time/step:	100 μ s, typical.
Accuracy & Stability:	Same as in CW when leveled at each step during dwell time.
Step Power Sweep Modes:	
Start/Stop:	$LA \leq [L1 \neq L2] \leq LB$ Sweeps up or down from a preset start level (L1) to a preset stop level (L2).
Start/ Δ :	$LA \leq [L1 \pm \Delta L] \leq LB$ Sweeps up or down from a preset start level (L1) through a preset sweep width (ΔL).
Ctr/ Δ :	$LA \leq [CL \pm (\Delta L/2)] \leq LB$ Sweeps up or down through a preset sweep width (ΔL) centered symmetrically about a preset center level (CL).
Start/Steps:	$LA \leq [L1 \pm (\text{step size} \times \text{number of steps})] \leq LB$ Sweeps up or down from a preset start level (L1) through a preset number of level steps.
Step Power Sweep Functions:	
Auto:	Continuous cycle of the preset sweep.
Single:	A single cycle of the preset sweep or (with stop activated) a single preset step, initiated the front panel pushbutton or receipt of the corresponding GPIB command.
Ext:	A single cycle of the preset sweep or (with stop activated) a single preset step, initiated by a trigger input from an external source.
Manual:	Stops the sweep when activated by the front panel pushbutton, the assertion of the Stop Sweep I/O BNC, or reception of the corresponding GPIB command to enable manual adjustment of the level at any point in the sweep. Permits continuation from the current level.

Modulation Parameters and Operational Modes

Option 24 provides two function generators for internal generation of amplitude and frequency modulation envelope waveforms. A pulse generator is also provided (Modes: free-run, triggered, gated, delayed, single, double, triple and quadruple).

Pulse/Square Wave Modulation (PM)

PM Envelope Parameters:

Specifications apply with Scan/AM and FM off. PM may be operated with FM and/or Scan.

On/Off Ratio: >80 dB at +10 dBm.

Rise/Fall Times:

Rise Time	Frequency Range
< 10 ns	> 500 MHz
< 50 ns	> 64 to 500 MHz
< 350 ns	25 to 64 MHz
< 500 ns	< 25 MHz

Overshoot, Undershoot and Ringing:

<10%, >500 MHz, maximum.

Settling Time:

<75 ns to within 1 dB (for pulses > 75 ns).

Leveled Pulsed Output Power:

Referenced to CW output power at 15 to 35 °C: ± 0.5 dB, ≥ 100 ns pulse width, ± 1 dB pulse width, between 100 ns and 75 ns.

Minimum Width	Frequency Range
20 ns	> 500 MHz
100 ns	64 to 500 MHz
1 μ s	< 25 to 64 MHz

Internally Generated PM Envelope (Option 24):

Repetition Rate:

Range	Resolution
1 Hz to 1000 Hz	1 Hz
1 kHz to 10 kHz	10 Hz
10 kHz to 100 kHz	100 Hz
100 kHz to 1MHz	1 kHz
1 MHz to 3 MHz	10 kHz

Pulse Start Delay:

Referenced to sync output.

Range: 50 ns to 1.67 sec.

Resolution: 10 ns.

Accuracy: $\pm 1\%$ of setting, or ± 20 ns, whichever is greater.

Jitter: $\pm 0.01\%$ of setting or ± 100 ps, whichever is greater.

Pulse Width:

Range: 100 ns to 1.67 sec.

Resolution: 10 ns.

Accuracy: $\pm 1\%$ of setting or 20 ns, whichever is greater.

Jitter: $\pm 0.01\%$ of setting or 100 ps, whichever is greater.

Pulse Modes: Triggered singlet, doublet, triplet, quadlet and free run.

Intervals:

Range: 100 ns to 1.67 sec.
Resolution: 10 ns.
Accuracy: $\pm 1\%$ of setting or 20 ns, whichever is greater.
Jitter: $\pm 0.01\%$ of setting or 100 ps, whichever is greater.

Output: Sync TTL levels into a 50 Ω load.
50 ns pulse coincident with start delay.
Video TTL levels into a 50 Ω load.

Series 12000A Microwave Synthesizers

Externally Triggered PM Envelope:

	One envelope produced by each trigger supplied.
Repetition Rate:	5 Hz to 5 MHz.
Pulse Delay:	Set by internal delay control.
Pulse Width:	Set by internal width control.
Input Trigger Required:	Positive or negative-going TTL level trigger pulse, >20 ns wide.

Externally Generated PM Envelope:

	One envelope produced by each pulse supplied.
Repetition Rate:	5 Hz to 5 MHz, leveled output; dc to 10 MHz, unleveled output.
Pulse Delay:	50 ns, typical (output envelope leading edge referenced to input pulse leading edge).
Input Pulse Required:	Positive or negative-going TTL level trigger pulse, >50 ns wide (leveled output); ≥20 ns wide (unleveled output). Input impedance is 50 Ω.

Amplitude Modulation (AM)

Specifications apply with FM off; AM may be operated simultaneously with FM

AM Envelope Parameters:

Modulation Depth:	0 to 90%, typical, at 0 dBm output power.
Modulation Resolution:	1%.
Modulation Bandwidth:	DC to 150 kHz, ±3 dB at 0 dBm output.
Modulation Accuracy:	±10% of depth setting.

Externally Supplied AM Envelope:

Waveform:	Any waveform compatible with bandwidth considerations.
Input Sensitivity:	(AM depth control set to 100%) 1 V _{p-p} for 50% depth ±10% depth, at 1 kHz modulation rate.
Input Impedance:	600 Ω, nominal.

Internally Generated AM Envelope:

	(Option 24 only).
Waveform	Sine, square, sawtooth, or triangle wave.
Rate:	0.01 Hz to 1 MHz.
Resolution:	2.5 mHz.
Accuracy:	Same as timebase.

Scan Modulation

(Specifications apply with FM and PM off; Scan may be operated simultaneously with FM and/or PM).

Envelope Parameters:

Frequency of Operation:	0.01 to 20 GHz.
Scan Mode:	
Range:	0 to 60 dB at +10 dBm output power.
Resolution:	0.1 dB.
Sensitivity:	-10 dB/V in 1 dB increments.
Step Response:	< 1 μ s for 50 dB change > 1 GHz (<10 μ s below 1 GHz).
Frequency Response:	DC to 150 kHz, sine wave, 3 dB.
Linearity:	± 0.6 dB, 0 to -20 dB; ± 1 dB @ 20 to 60 dB.
Input Impedance:	600 Ω , nominal.
Accuracy:	.25 dB +/- 5% at depth in dB (for .01 to 2 GHz specification applies only up to 30 dB).

Frequency Modulation (FM)

Specifications apply with Scan/AM and PM off; FM can be operated simultaneously with Scan/Linear AM and/or PM (PM and linear AM are not allowed simultaneously).

FM Envelope Parameters:

Wide Mode:	
Max Deviation:	See following Table.
Minimum Deviation:	10 kHz at 4 to 8 GHz (other ranges proportional).
Modulation Resolution:	1 kHz (deviation <1 MHz); 10 kHz (deviation >1 MHz) at 4 to 8 GHz (other ranges proportional).
Flatness:	± 2 dB for rates from 100 Hz to 1 MHz; ± 3 dB to 8 MHz.
Residual FM:	See following table.

Series 12000A Microwave Synthesizers

Narrow Mode:

Max Deviation:	See following Table.
Modulation Resolution:	10 Hz (deviation <10 kHz); 1 kHz (deviation >10 kHz) at 4 to 8 GHz (other ranges proportional).
Flatness:	± 2 dB for rates from DC to 1 MHz.
Residual FM:	Same as CW.

Both Modes:

Modulation Accuracy:	+5%, at maximum deviation and 1 kHz modulation rate.
Distortion:	<5% (± 1 MHz deviation); 4 to 8 GHz range.
Incidental AM:	$\pm 0.2\%$ /MHz of deviation.

Frequency (GHz)	Max Wide Deviation (Peak)	Max Narrow Deviation (Peak)	Wide Mode Residual FM
.010 to .016	40 kHz	2 kHz	200 Hz
.016 to .032	80 kHz	4 kHz	200 Hz
.032 to .064	160 kHz	8 kHz	200 Hz
.064 to .125	320 kHz	16 kHz	200 Hz
.125 to .25	640 kHz	32 kHz	200 Hz
.25 to .5	1.25 MHz	64 kHz	200 Hz
.5 to 1	2.5 MHz	125 kHz	375 Hz
1 to 2	5 MHz	250 kHz	<750 Hz
2 to 4	10 MHz	.5 MHz	<1.5 kHz
4 to 8	20 MHz	1 MHz	<3 kHz
8 to 16	40 MHz	2 MHz	<6 kHz
16 to 20	80 MHz	4 MHz	<12 kHz

Internally Generated FM Envelope:

(Option 24 only).

Waveform:	Sine, square, sawtooth, or triangle wave.
Rate:	0.01 Hz to 1 MHz.
Resolution:	2.5 mHz.
Accuracy:	Same as timebase.
THD:	1% typical.

Externally Supplied FM Envelope:

Waveform:	Any waveform compatible with bandwidth considerations.
Rate:	DC to 8 MHz Narrow Mode, 100 Hz to 8 MHz Wide Mode.
Input Sensitivity:	Settable; 1 Vp input for maximum peak deviation (FM deviation control set to maximum).
Input Impedance:	50 Ω , nominal.

1.3 General Specifications

Remote Interface:	IEEE STD 488.2 for all parameters except AC power on/off. RS-232 Serial Interface DB9 connector.
Operating Temperature:	0 to 55 °C.
Environmental:	Complies with MIL-PRF-28800F, Class 3.
Approvals:	CE marked.
Power:	90 to 253 Vac, auto-sensing, 47 to 64 Hz (400 Hz optional), 200 Watts, nominal.
Line Fuse Rating:	2 A, Slo-Blo, 250V, Type T.
Dimensions:	13.3 cm high x 42.5 cm wide x 53.3 cm deep. (5.25 in H x 16.75 in W x 21 in D)

Performance Tests

2.1 Introduction

This chapter provides step-by-step procedures to verify performance of the Series 12000A Microwave Synthesizers.

The required warm-up time before testing is 72 hours. The warm-up period can be reduced to 30 minutes if timebase accuracy is not to be tested.

In these procedures, the instrument being tested may be referred to as the 12000A or UUT (Unit Under Test).

2.1.1 Recommended Equipment

The following equipment is recommended before starting the performance test routines (the recommended equipment can be substituted provided the specifications are sufficiently compatible):

- Frequency Standard, 10 MHz
- Oscilloscope, Tektronix 2465 or equivalent
- Microwave Frequency Counter, Systron Donner 6245B or equivalent
- Power Meter and Sensor, Giga-tronics 8541A/8651A with 80313A sensor, or equivalent
- Spectrum Analyzer, HP 8566B or equivalent
- Detector, Herotek Model DZ262-44 or equivalent
- Function (Audio) Generator, Wavetek 191 or equivalent
- Measuring Receiver, HP 8902A or equivalent
- Distortion Analyzer, HP 339A or equivalent
- L.O. Generator, Giga-tronics Microwave Synthesizer
- Universal Counter, Racal Dana 1994 or equivalent
- Mixer IF Amplifier with Divide-by-40 output
(Giga-tronics Mixer/Divider, Part Number 002CA04900)

2.2 Performance Tests

2.2.1 Introduction

The procedures in this section verify the electrical performance of the 12000A using the specifications in Chapter 1.

Each of the performance tests includes a list of recommended test equipment. There is a consolidated list at the beginning of this chapter. Equivalent test equipment can be substituted provided that the accuracies and specifications are sufficiently compatible.

A test data sheet is included for you to enter the various readings taken. The specification and tolerance range is listed for ease of verification. It is suggested that copies be made of the manual sheets. When automated tests are run, a printed data sheet is produced.

Performance verification is recommended at least every two years, or more often when required to ensure proper operation of the instrument.

Each procedure specifies a required warm-up time if the procedure is to be done individually. Only one warm-up period is required for a sequence of tests. Test equipment must be warmed up according to specifications.

2.2.2 Frequency Range, Resolution and Accuracy

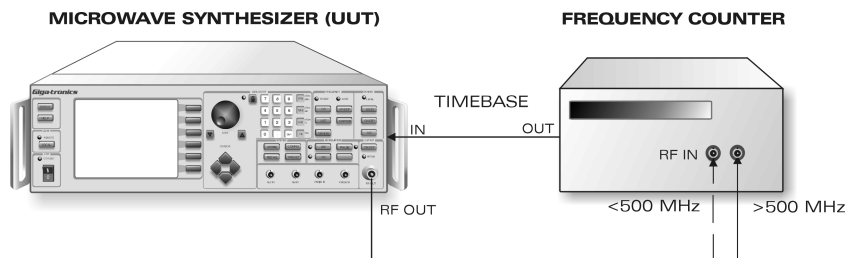
Description:

Connect the 12000A RF output to the input of a frequency counter. The internal time base of the counter is a reference for the 12000A to eliminate time base errors from the measurements. This procedure does not check for time base accuracy, and therefore the frequency in the 12000A display should agree with the counter, within the resolution of each instrument.

It is possible for a fault in the 12000A to cause a frequency error even though the lock indicators show normal operation. For this reason a number of specific frequencies are tested. Test frequencies have been selected so that any defective circuits will be easily isolated.

Equipment Required:

UUT • Frequency Counter • Coaxial Cable



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Figure 2-1: Frequency Range, Resolution and Accuracy

Procedure:



NOTE: Steps 1 through 4 are used only for instruments operating down to 10 MHz.

1. Connect the equipment as shown in Figure 2-1. Connect the 12000A RF Output to the 10 to 500 MHz counter input using the coaxial cable and the SMA to BNC adapter. Allow the equipment to warm up for at least 30 minutes. Because the 12000A and the counter use the same time base, time base errors are eliminated. The 12000A will automatically switch to the external reference when it is connected.
2. Set the 12000A to 10 MHz. Press **[LEVEL]** in the POWER field and enter **[−] [1] [0] [dBm]**. Press **[RF ON]** in the RF OUTPUT field to turn on the RF output.
3. Set the 12000A to each frequency listed on the data sheet and verify that the counter reads the set frequency plus or minus the counter resolution. This tests each divider stage.
4. Connect the 12000A RF Output to the 500 MHz to 26.5 GHz input on the counter, and continue with the divider tests.
5. To check that the multipliers are functioning properly, refer to the test data sheet and program each of the listed frequencies into the 12000A by entering (for example) **[CW] [2] [0] [0] [1] [MHz]**. For each listed frequency the counter should read the entered frequency ± 1 Hz, plus or minus the counter resolution. Ignore all frequencies outside the range of the instrument under test.

2.2.3 Spurious Signals Tests

Description:

The output of the 12000A is connected to a spectrum analyzer. Various frequencies are selected and the analyzer tuned to determine the presence of either harmonically or non-harmonically spurious signals.

Equipment Required:

UUT • Spectrum Analyzer • Coaxial Cable

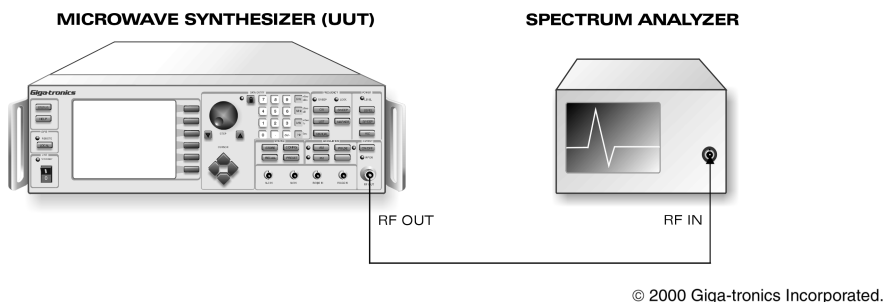


Figure 2-2: Spurious Signals Tests

Procedure:

1. Connect the equipment as shown in Figure 2-2. Allow the equipment to warm up for at least 30 minutes. Press **[CW]** in the FREQUENCY field on the 12000A and enter the first test data sheet frequency within the range of the 12000A. The RF amplitude should be at +6 dBm. Press **[RF ON]** to turn on the RF output. Be certain that all modulation is OFF.
2. Set the spectrum analyzer to view the 12000A output signal. Adjust the analyzer reference level so that the peak of the displayed signal is at the top graticule line.
3. Set the spectrum analyzer to maximum span with the signal centered on the screen. Gradually narrow the span, keeping the signal centered, to observe any spurious signals. Use appropriate resolution and video bandwidths to allow sufficient dynamic range.
4. Repeat steps 2 and 3 for the other frequencies on the test data sheet which are within the operating range of the instrument.

Many spectrum analyzers have a tuned preselector when the frequency is above about 2 GHz. This reduces the likelihood of analyzer generated spurious signals, but does not eliminate the possibility. If in doubt, increase the RF attenuation of the analyzer by 10 dB. The signal in question should be reduced by exactly 10 dB. If not, it is analyzer generated. It is also important for frequencies below the range of the preselector that sufficient analyzer RF Attenuation be used (typically 30 dB) to avoid the analyzer generating harmonics of the input signal. The above attenuator shift technique will also allow verification of harmonic levels.

If a spurious signal appears to be out of specification, first check that the fundamental signal level is at +6 dBm. Next verify the analyzer accuracy by connecting a known amplitude signal (from the 12000A, for example) at the spurious frequency.

The adjusting knob on the 12000A may generate some noise spikes when it is rotated. The acquisition of the various phase lock loops in the instrument can also cause transients (within the specified settling time). Both of these effects will disappear when a steady state condition has been reached.

It is important to identify the particular class of spurious signal as the specifications may be different for each. If the spurious signal is an exact multiple of the 12000A RF output then the harmonic specification applies. Any other spurious signals must meet the non-harmonically related specification.

For frequencies above the fundamental range of the spectrum analyzer, either a mixer supplied with the spectrum analyzer or an external mixer and local oscillator may be used to downconvert the signal. Care must be taken to identify spurious signals which are inherently generated by the mixing process.

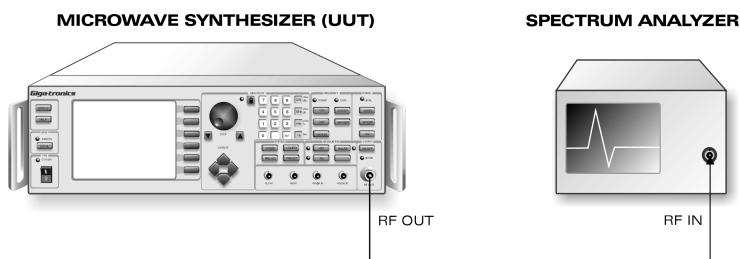
2.2.4 Single Sideband Phase Noise

Description:

The test in this procedure is limited by the measuring system and verifies only the majority of the phase noise specification. To completely test the phase noise specification requires a far more sophisticated measurement system. This test uses the spectrum analyzer to make all measurements from 100 Hz to 1 MHz offsets. The 100 Hz and 1 MHz offsets are particularly susceptible to measurement system limitations.

Equipment Required:

UUT • Spectrum Analyzer • Coaxial Cable



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Figure 2-3: Single Sideband Phase Noise

Procedure:

1. Connect the 12000A RF output to the spectrum analyzer input. Place the 12000A on a foam pad to isolate it from any external mechanical vibrations, which could affect the phase noise measurement.
2. Turn off all modulation on the 12000A.
3. For the first frequency on the test data sheet within the range of the instrument, press **[CW]** and enter the frequency. Tune the spectrum analyzer to the generator frequency and adjust the 12000A RF level to obtain a reference of 0 dBm on the analyzer. This allows direct measurement of the phase noise by the analyzer.
4. Set the analyzer span such that the desired offset is at ± 2 divisions, select an appropriate bandwidth, activate the phase noise measurement and place the marker two divisions to the right of the carrier. Read the phase noise in dBc/Hz. Repeat for all offsets.
5. Repeat steps 3 and 4 for the other test data sheet frequencies which are within range of the 12000A.

2.2.5 RF Output Power Tests

Description:

Although it is possible to make the following measurements manually, it is extremely tedious. It is recommended that an automated system be set up to take and record the data. Three tests are run. The first measures the maximum available output with the level control loop disabled. The second verifies the accuracy and flatness across the operating frequency range at a fixed output (0 dBm). The remaining test checks the step attenuator accuracy at a number of frequencies. This section outlines the general procedure followed by the automated system, a similar measurement could be done manually.

Equipment Required:

UUT • Local Oscillator • Measuring Receiver & Sensor • Downconverter • Plotter • Computer and Programs

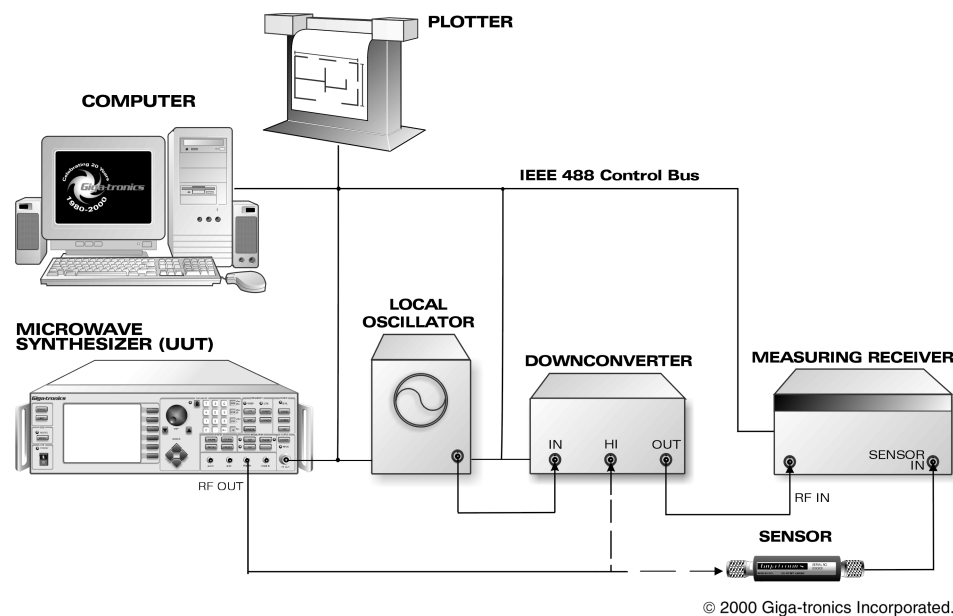


Figure 2-4: RF Output Power Tests

Procedure:

1. Connect the power sensor to the 12000A. Disable the leveling system of the 12000A. Step the frequency across the particular instrument operating range in 50 MHz increments. At each point measure the power, apply the appropriate sensor correction factor, and plot the result.
2. Using the above setup, set the 12000A to 0 dBm with the leveling enabled. Again, step the frequency across the operating range; measure, correct, and plot the power.
3. *For instruments with Option 26:*
Connect the 12000A to the measuring receiver via the downconverter. With the 12000A at 0 dBm and set to the first test frequency, establish a reference on the receiver. Reduce the 12000A output in 10 dB steps, observing and recording the receiver reading. As needed, perform the recalibration requested by the receiver.
4. Repeat this procedure for the remaining test frequencies.

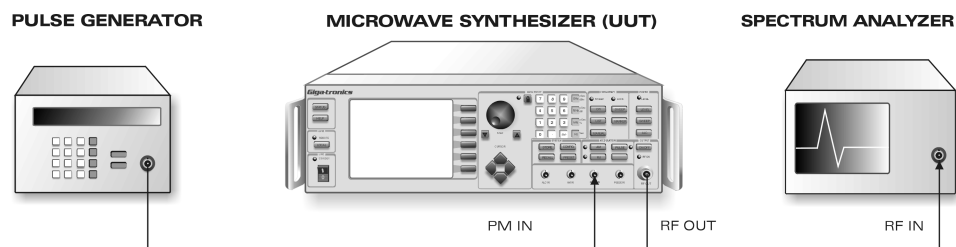
2.2.6 Pulse Modulation On/Off Ratio Test

Description:

The 12000A is set to a CW frequency at a power level of 0 dBm. A spectrum analyzer is used to view the signal. The pulse modulation is then enabled and the resulting waveform is measured.

Equipment Required:

UUT • Spectrum Analyzer • Pulse Generator • Coaxial Cable



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Figure 2-5: Pulse Modulation On/Off Ratio Test

Procedure:

1. Connect the equipment as shown in Figure 2-5. Allow 30 minutes warm-up time.
2. Enter the first frequency on the test data sheet within the frequency range of the instrument. The RF power level should be at 0 dBm. Select external pulse modulation (PM) on the 12000A.
3. Tune the analyzer to the source frequency, select an analyzer span of 0 Hz and fine tune the analyzer to place the line at the top of the screen graticule (adjust analyzer reference level as needed).
4. Set the pulse generator for a 100 Hz square wave; press **[PULSE]** then use the softkey to turn on the pulse modulation.
5. Adjust the analyzer sweep time to display a few cycles of the waveform. Use internal triggering. Reduce resolution bandwidth and carefully retune the analyzer center frequency until the maximum resolution is achieved. Read and record the peak-to-peak value (use marker delta).
6. Repeat steps 3, 4 and 5 for all other test data sheet frequencies which are within the range of the instrument. Note that the dynamic range of the analyzer may limit its measurement capability.

2.2.7 Pulse Modulation Rise and Fall Time Test

Description:

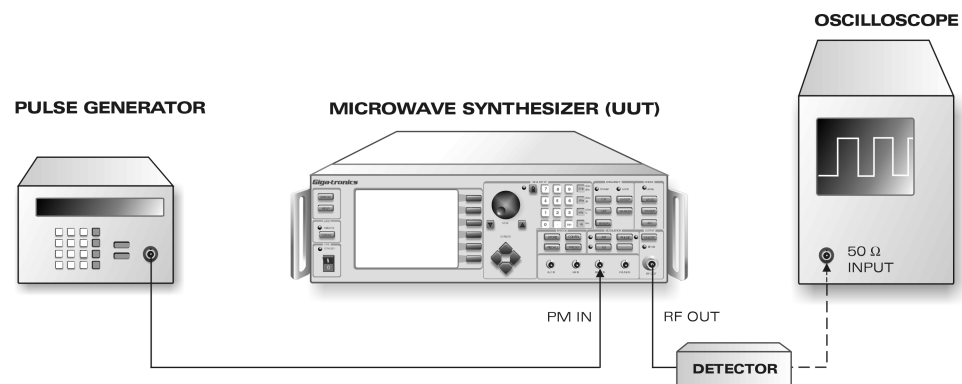
A crystal detector is connected to the 12000A, terminated in 50 Ω , and monitored with an oscilloscope.



NOTE: It is very important to use either the specified detector or one with similar rise time characteristics. Even when terminated in 50 Ω with a short cable, the detector parameters can markedly influence the measurement.

Equipment Required:

UUT • Oscillator • Pulse Generator • Crystal Detector • Coaxial Cable



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Figure 2-6: Pulse Modulation Rise/Fall Time Test

Procedure:

1. Connect the equipment as shown in Figure 2-6. The cable from the detector to the oscilloscope should be kept as short as possible.
2. Press **[PRESET]** on the 12000A and set the frequency to the first test data sheet frequency within the operating range of the instrument.
3. Enable external pulse modulation (at a 1 MHz rate and 0.5 μ s width) on the 12000A. Press **[PULSE]** and use the softkey to turn on pulse modulation.
4. Set the oscilloscope to 5 mV/div and using the RF Level control of the 12000A, adjust the peak to peak oscilloscope display to fall on the dotted lines on the screen (100% and 0%). Adjust the oscilloscope sweep time to 5 ns/div. Measure and record the rise and fall times between the 10% and 90% points.
5. Repeat Step 4 for each of the test data sheet frequencies within the operating range of the instrument.

2.2.8 Pulse Modulation Overshoot and Settling Time

Description:

A crystal detector is connected to the 12000A, terminated in 50 Ω , and monitored with an oscilloscope.

NOTE: It is very important to use either the specified detector or one with similar rise time characteristics. Even when terminated in 50 Ω with a short cable, the detector parameters can markedly influence the measurement.

Equipment Required:

UUT • Oscillator • Pulse Generator • Crystal Detector • Coaxial Cable

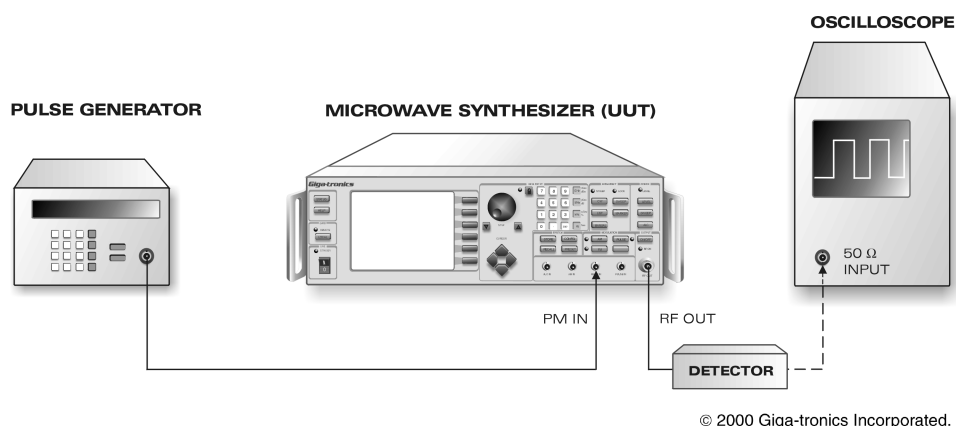


Figure 2-7: PM Overshoot and Setting Time

Procedure:

1. Connect the equipment as shown in Figure 2-7. The cable from the detector to the oscilloscope should be kept as short as possible.
2. Press **[PRESET]** on the 12000A and set the frequency to the first test data sheet frequency within the operating range of the instrument.
3. Enable external pulse modulation (at a 1 MHz rate and 0.5 ms width) on the 12000A. Press **[PULSE]** and use the softkey to turn on pulse modulation.
4. Set the oscilloscope to 5 mv/div and using the RF Level control of the 12000A and the vertical position of the oscilloscope, adjust the peak to peak oscilloscope display to be from the top of the screen (pulse off) to 2 divisions below the center line (pulse on). Adjust the oscilloscope sweep time to 50 ns/div. Change the level setting of the 12000A by plus and minus 1 dB and note the graticule position of the pulse on level. Return to the original value. Measure and record the time for the pulse to be within 1 dB of its final value.
5. Change the level setting of the 12000A by plus and minus 2 dB and note the graticule position of the pulse on level. Return to the original level. Measure and record any undershoot/overshoot of the signal.
6. Repeat Steps 4 and 5 for each of the test data sheet frequencies within the operating range of the instrument.

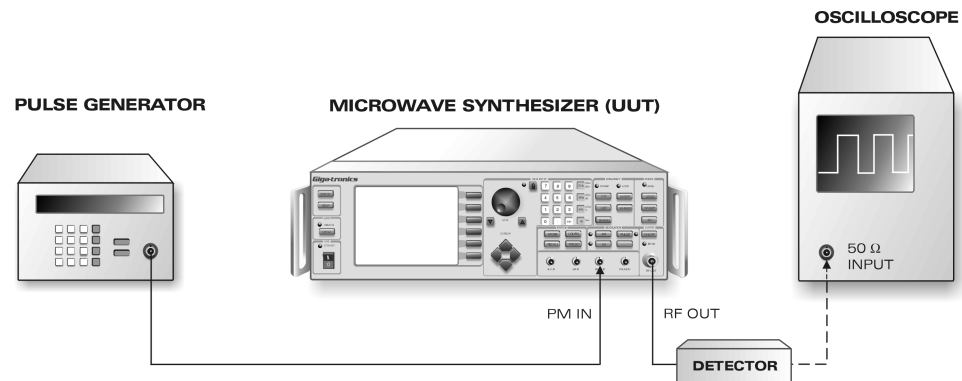
2.2.9 Pulse Modulation Accuracy Test

Description:

In this test the peak pulse level is compared to the level in the CW mode.

Equipment Required:

UUT • Oscilloscope • Pulse Generator • Crystal Detector • Coaxial Cable



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Figure 2-8: Pulse Modulation Accuracy Test

Procedure:

1. Connect the equipment as shown in Figure 2-8. The oscilloscope input impedance should be 50 Ω . Allow 30 minutes warm-up.
2. Press **[PRESET]** on the 12000A and set the frequency to the first test data sheet frequency within the operating range of the instrument.
3. Set the oscilloscope to 5 mv/div and using the vertical position of the oscilloscope, adjust the trace to the centerline of the screen. Change the level setting of the 12000A by plus and minus 1 dB and note the trace position on the screen. Return to 0 dBm.
4. Enable external pulse modulation (at a 200 kHz rate and 0.1 μ s width) on the 12000A. Press **[PULSE]** and use the softkey to turn on pulse modulation.
5. Measure and record the difference between the CW reference level and the negative peak of the pulse.
6. Change the pulse width to 50 ns and again measure and record the difference between the CW reference level and the negative peak of the pulse.
7. Repeat Steps 3-6 for each test data sheet frequency within the operating range of the instrument.

2.2.10 Frequency Modulation Tests

Description:

The output from the 12000A is connected to a discriminator. The discriminator output is monitored on an oscilloscope to determine deviation and bandwidth.

Equipment Required:

UUT • Function Generator • Oscilloscope • Digital Voltmeter • FM Test Fixture

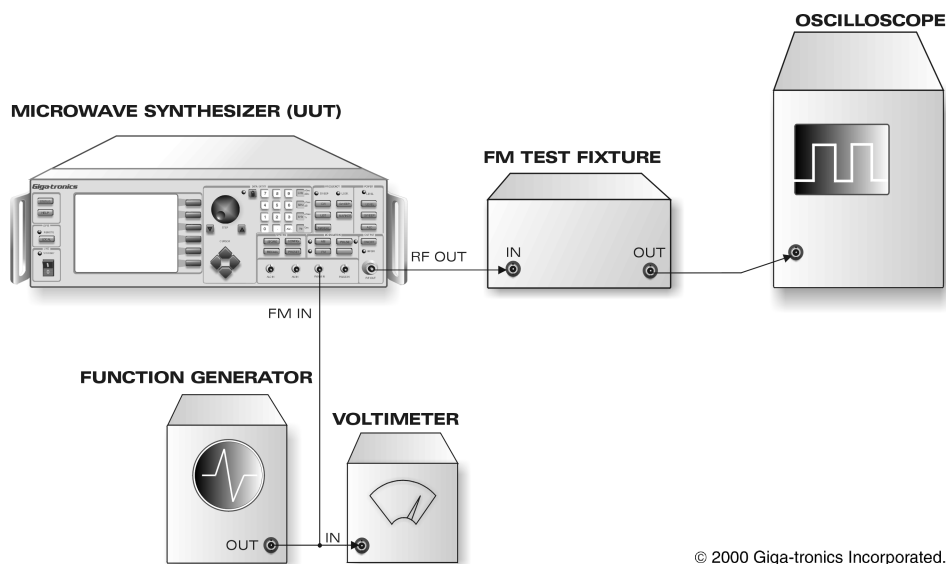


Figure 2-9: Frequency Modulation Test

Procedure:

In order to calibrate and test the frequency modulation circuits, a special test fixture must be assembled. The recommended FM test fixture includes an RF splitter, two lines of unequal length, and an RF mixer. The RF output of the 12000A is divided by the splitter into two signals, unequally delayed. The required differential delay can be obtained by using two coaxial cables of, for example, 5 and 10 inches in length. The outputs of these delay lines are furnished to the two inputs of the RF mixer. For certain frequencies, which may be identified by experiment, the mixer will produce a DC voltage near zero. The number of null frequencies can be increased by making the delay lines longer in absolute terms or by increasing the ratio between their lengths. If the output becomes frequency modulated, the mixer output voltage will change, and the voltage variation will be proportional to FM deviation. The polarity of the voltage change may be either directly or inversely related to the direction of frequency deviation. When voltage levels have been established for different frequencies, the mixer output can be monitored on an oscilloscope to provide a continuous display of FM deviation.

1. Connect the FM test fixture to the RF OUT connector of the 12000A as shown in Figure 2-9. Monitor the mixer output with the oscilloscope (5 mV/div). Set the 12000A to any null frequency between 4.0 and 7.99 GHz (that is, at a frequency where the mixer output voltage is zero); +10 dBm out, no modulation.
2. Establish the voltage at 1 MHz above and 1 MHz below the null frequency. Adjust the oscilloscope gain and the 12000A output power level (near +5 dBm) to place the null point at the center of the screen and the 1 MHz deviation points at 3 divisions above and 3 divisions below the null point.

3. Set the 12000A to Narrow EXT FM with 1 MHz deviation. Connect the function generator, set to a 100 kHz rate SINE wave, 2 V_{pp}. Verify that the waveform is 6 divisions peak-to-peak (± 0.3 divisions).
4. Adjust the 12000A FM deviation for exactly a six division peak-to-peak display. Vary the function generator from 10 Hz to 1 MHz and verify that the display remains between five and seven divisions peak-to-peak.
5. Vary the function generator from 1 MHz to 8 MHz and verify that the display remains between 4 and 8 divisions.
6. Establish the voltage at 10 MHz above and below the null frequency. Adjust the oscilloscope gain and the 12000A output power level (near +5 dBm) to place the null point at the center of the screen and the 10 MHz deviation points at 3 divisions above and 3 divisions below the null point (terminate the Mixer output in 50 Ω).
7. Set the 12000A to Wide EXT FM with 10 MHz deviation. Set the function generator to 100 kHz. Verify that the waveform is 6 divisions peak-to-peak (± 0.3 divisions).
8. Adjust the 12000A FM deviation for exactly a 6-division peak-to-peak display. Vary the function generator from 100 Hz to 1 MHz and verify that the display remains between 5 and 7 divisions.
9. Vary the function generator from 1 MHz to 8 MHz and verify that the display remains between 4 and 8 divisions.

Series 12000A Microwave Synthesizers

Series 12000A Test Data Sheet

(Page 1 of 2)

Serial Number:		Under Test Result record measured values (if any). In the case of a function check or range check, write OK to indicate that the unit under test meets specifications.
Date:		
Tested By:		
Quality Assurance:		

Frequency Range, Resolution, Accuracy		Test Result
4.2.2.3	12 MHz	
	24 MHz	
	48 MHz	
	100 MHz	
	200 MHz	
	400 MHz	
4.2.2.4	750 MHz	
	1500 MHz	
	3 GHz	
4.2.2.5	6 GHz	
	12 GHz	
	18 GHz	

Spurious Signals Tests		
Frequency (MHz)	Harmonics	Non-Harmonics
770.550		
1513.425		
4004.000		
9182.433		
17361.522		

Series 12000A Test Data Sheet (Page 2 of 2)

Serial Number:		Tested By:	
Date:		Quality Assurance:	

Single Sideband Phase Noise (dBc/Hz)					
Frequency (MHz)	Offset from Carrier				
	100 Hz	1 kHz	10 kHz	100 kHz	1 MHz
1513.425					
4004.000					
9182.433					
17361.522					
23541.349					

RF Output Power		Test Result
Max. Power Level		
Power Level		
Step Attenuator test frequencies	1.0 GHz	
	4.0 GHz	
	12.0 GHz	
	17.0 GHz	

Pulse Modulation Tests					
Frequency (GHz)	On/Off	Rise/Fall	Overshoot	Settling	Accuracy
1.0					
4.0					
12.0					
20.0					

Frequency Modulation Tests					
Parameter		@1 GHz	@4 GHz	@12 GHz	@20 GHz
4.2.10.3	Deviation (5.7 - 6.3 div)				
4.2.10.4	Bandwidth (5 - 7 div)				
4.2.10.5	Bandwidth (4 - 8 div)				
4.2.10.7	Deviation (5.7 - 6.3 div)				
4.2.10.8	Bandwidth (5 - 7 div)				
4.2.10.9	Bandwidth (4 - 8 div)				

Adjustments

3.1 Introduction

The model 12000A features completely 'closed case' calibration. There are no mechanical adjustments anywhere in the instrument and all calibration is done under computer program control. Prior to performing any of the calibration procedures, allow the instrument to operate for at least 30 minutes. The calibration process is divided into sections of related steps. Each section should be performed in its entirety.

The Calibration Control Program runs on a Pentium based Windows 95, 98[®] PC. Please refer to the addendum to this section for details on installing and running this program.

3.2 Recommended Test Equipment

The following equipment is recommended/required to properly calibrate the model 12000A. Where the word "required" appears, the exact equipment specified must be used due to the need for proper computer control.

- Personal computer (PC) with Pentium CPU running Windows 95, 98[®], 1.44 MB Floppy disk drive, CEC488 (Capital Equipment Corp) IEEE 488 interface.
- Giga-tronics 8651A or 8652A power meter **(Required)**
- Giga-tronics 80313A Low VSWR sensor **(Required)**
- Male "N" to female "K" adapter
- DC voltage source (0-10 volts)
- Digital voltmeter, 3 ½ digit
- Audio source, 10 Hz to 200 kHz, 2 V_{pp} into 50 Ω output
- Agilent 8902 Modulation Analyzer **(Required)** with downconverter.
- 10 MHz (5 MHz is also acceptable) frequency standard.

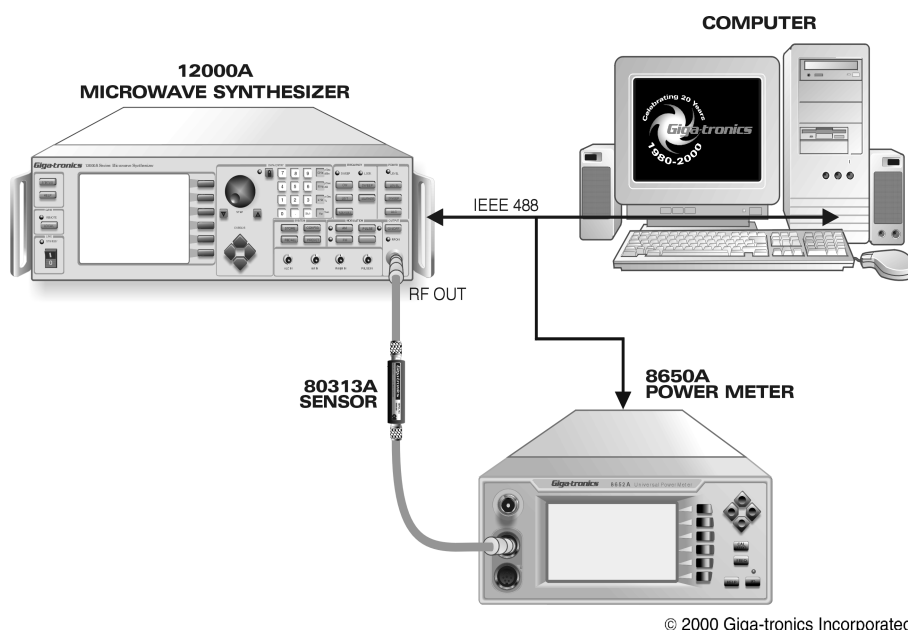
3.3 Time Base Calibration

The time base oscillator used in the 12000A operates at a frequency of 10 MHz and uses Electronic Frequency Control to adjust its output frequency. The calibration is performed entirely by the 12000A without the need for an external computer. Prior to performing this calibration the instrument should be connected to the mains for at least 24 hours (48 hours for option 28). It is not necessary to have the instrument on. Note that the accuracy of the calibration is directly related to the accuracy of the external standard.

1. Turn on the instrument and allow a 30 minute warm-up.
2. Connect the frequency standard to the rear panel 'Ref In' BNC connector.
3. Press the **'Config'** button, then the **'Service'** softkey, then the **'Hardware Testing'** softkey, then the **'Time Base Cal'** softkey.
4. Either a 5 or a 10 MHz reference frequency may now be selected using the up/down buttons.
5. Press the **'Cal'** softkey and then the key to store the calibration.

3.4 Output Amplitude Calibration

There are five steps in this section. These steps provide data that the instrument ALC system needs to properly control the control amplitude. The steps **must** be performed in the order specified. The entire process is managed by the Calibration Control Program running on the PC. Please read the section which describes the individual test for information on when re-calibration is necessary.



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Figure 3-1: Output Amplitude Calibration Connection

1. Connect the sensor to the meter calibrator (use the 'N' to 'K' adapter) and allow at least 15 minutes for the sensor and meter to reach thermal equilibrium. Then perform a sensor calibration.
2. Now connect the equipment as shown above. The 80313A sensor connects to the 12000A RF out connector. If the 12000A has a type 'N' connector, use the 'N' to 'K' adapter. The 12000A should have its IEEE address at 6 (the default). The power meter should be at address 10.

If the 12000A has not been previously warmed up, allow 30 minutes of warm-up. When the 'Fixed Frequency' screen displays, press the **RF On** button.

3. Start the Calibration Control Program as described in the addendum to this section.

The initial program window has four sections

The Setup section displays the UUT address, set to 6, the default address for the 12000A. It also shows the power meter address, set to 10.

The Parameter Block section shows a number of characteristics for the instrument. The data for these characteristics are displayed after the "Read Parameters" button is clicked (see directions below).

The Characterize section serves as the means to run the calibration routines. Only the ALC routines are included here. See the section on modulation calibration for the descriptions of the other routines.

- The 'Modulator' routine generates a curve of attenuation verses control voltage for the modulators at various frequencies. This section must be performed whenever the A3, A6, or A8 assemblies have been changed.
- The 'Detector' routine does the same for the detector output voltage verses output power. Perform this section if A3, A6, A8, or A17 has been changed. Be sure to do the 'Modulator' characterization first, if needed.
- 'Frequency Response' stores correction factors as a function of output frequency. This section will be required if A6, A8, or the optional step attenuator has been changed. It is also recommended that this routine be run if any of the RF cables between A6 and the front/rear output or the output connector is changed. Be sure to do both the 'Modulator' and the 'Detector' characterizations (in that order) first, if required.
- 'Attenuator' stores correction factors as a function of the step attenuator position and frequency. This data is supplied by the attenuator manufacturer on a disk. Replacing an attenuator requires using the supplied data and performing this section. Attenuator replacement also requires that the 'Frequency Response' characterization be performed.

3.4.1 ALC Characterization Instructions

The following is a description of the ALC characterization portion of the Calibration Control Program operation. In addition, there are on screen prompts during the execution of various routines. The sequence shown covers all of the routines. You may select those that need to be performed. Be sure to maintain the overall order.

- Click **'Read Parameters'**. This will interrogate the 12000A and fill in the data on the screen.
- In the Characterize section, click on the 'Modulator (AM/PM)' box.
 - The routine will take between 30 and 45 minutes, depending on the instrument frequency range.
 - When the routine completes, power down the 12000A and restart it. This is the equivalent of "In order for the changes to take effect you must restart your computer"! Once the 'Fixed Frequency' screen appears, press 'RF On'.
- Click **'Read Parameters'**. This will interrogate the 12000A and fill in the data on the screen.
- In the Characterize section, click on the 'Detector' box.
 - The routine will take between 30 and 45 minutes, depending on the instrument frequency range.
- In the Characterize section, click on the 'Frequency Response' box.
 - The routine will take between one and three hours, depending on the instrument frequency range.
- In the Characterize section, click on the 'Attenuator' box.
 - The routine will take about 5 minutes.

3.5 Modulation Calibration

There are three separate calibration routines for the modulation functions of the 12000A. Each requires a different test setup. See the following sections for a complete description of the test system and sequence. Modulation calibrations may be done in any order. The conditions requiring re-calibration are outlined in this description of the Characterization screen of the Calibration Control Program:

- 'FM Calibration' performs the necessary steps to calibrate the frequency modulation function. FM calibration must be done if the A1 synthesizer board is replaced.
- 'AM Calibration' performs the necessary steps to calibrate the amplitude modulation function. This calibration should be performed whenever the A3, A6, or A8 assemblies are replaced. Be sure to do both the 'Modulator' and the 'Detector' characterizations (in that order) first, if required.
- 'Modulator (Scan)' calibrates and linearizes the modulators to allow the open loop 'deep' AM (Scan Modulation). This calibration should be performed whenever the A3, A6, or A8 assemblies are replaced. Be sure to do both the 'Modulator' and the 'Detector' characterizations (in that order) first, if required.

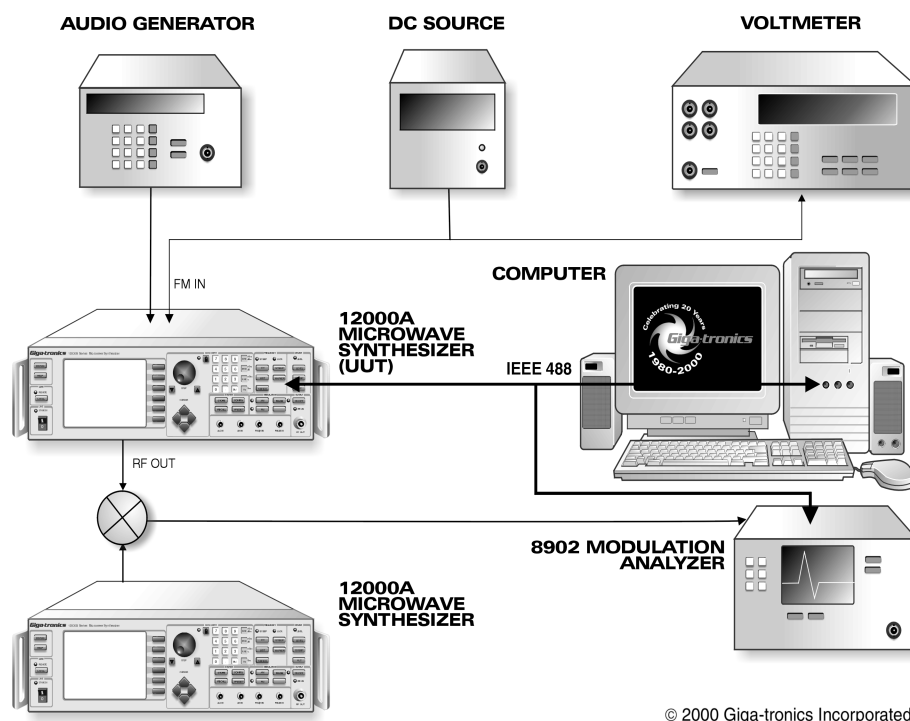


Figure 3-2: Frequency Modulation Calibration Connection

Connect the UUT, computer, and Modulation Analyzer to the IEEE 488 bus. The UUT should be at address 6 (the default). Connect the UUT RF output to the mixer RF input and the L.O. source (shown as a second model 12000) to the mixer LO input. Set the L.O. source to 5130 MHz at +10 dBm, CW mode. Connect the mixer IF output to the Modulation Analyzer input. The step-by-step procedure below explains how to use the Audio Source DC Source and Voltmeter. Operator actions are directed by screen prompts.

If the 12000A has not been previously warmed up, allow 30 minutes of warm-up. When the 'Fixed Frequency' screen displays, press the **RF On** button.

Series 12000A Microwave Synthesizers

Start the Calibration Control Program as described in the addendum to this section.

Click '**Read Parameters**'. This will interrogate the 12000A and fill in the data on the screen.

- In the Characterize section, click on the 'FM Calibration' box.
- The first step requests a zero volts input to the UUT FM connector. Simply leave the input open as there is an internal 50Ω resistor to ground. This test calibrates any zero offset errors. Since FM is DC coupled, any DC component (or zero error) will result in a frequency shift. Press 'Continue' when ready.
- When the prompt requests a 1.0 volt DC input, connect the DC source to the FM input connector and monitor the FM input connector with the voltmeter. Set the DC source to 1.00 volts ± 0.005 volts. It may be helpful to put a resistor of about 500 ohms in series with the source and the FM input. This will make setting the DC source less critical as it provides a 10:1 divider. Be sure to measure the voltage at the FM input connector with everything connected. This test calibrates the "inside the loop" portion of the FM (approximately DC to 15 kHz). Press 'Continue' when ready.
- The next step requires that the 8902 Modulation analyzer be connected to the 12000A. Since the test is run at a frequency of 5 GHz, it is necessary to 'downconvert' the 12000A output to a frequency within the range of the 8902. A suitable downconverter may be built using a mixer and another source. Set the other source (LO) to 5130 MHz at +10 dBm and connect it to the mixer LO port. Connect the 12000A to the mixer RF port. Connect the mixer IF out to the 8902 input. Connect the audio source to the 12000A FM input. Set the source to 200 kHz at 2.00 Volts peak-to-peak ± 0.01 volts. An oscilloscope is **NOT** accurate enough to set this level. Use a calibrated source or a digital voltmeter which will accurately measure 200 kHz. This test calibrates the "outside the loop" portion of the FM (approximately 15 kHz to 8 MHz) Press 'Continue' when ready.

3.5.1 Amplitude Modulation Calibration

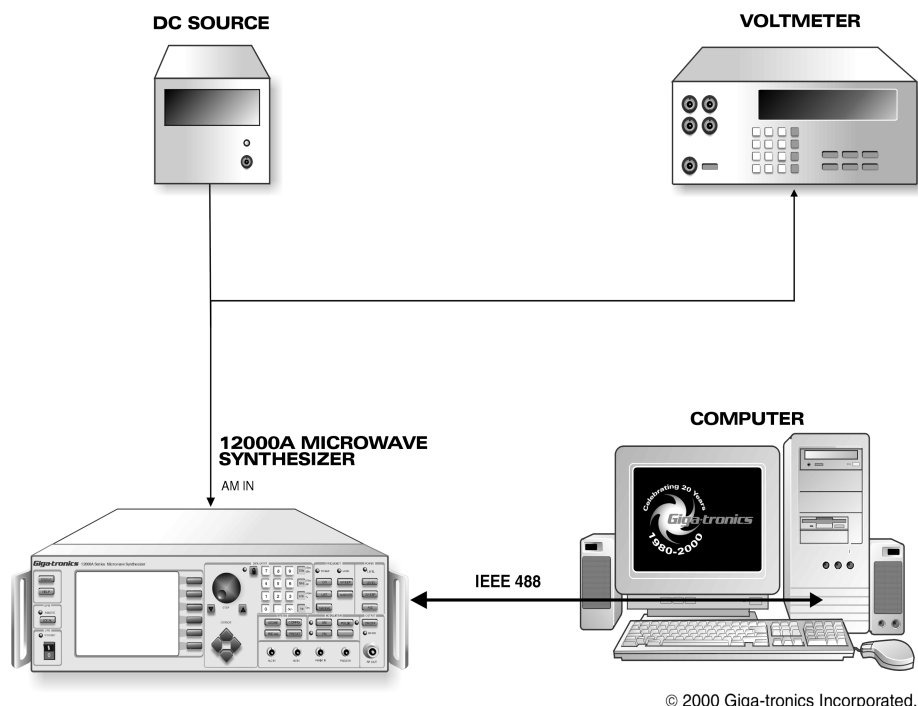


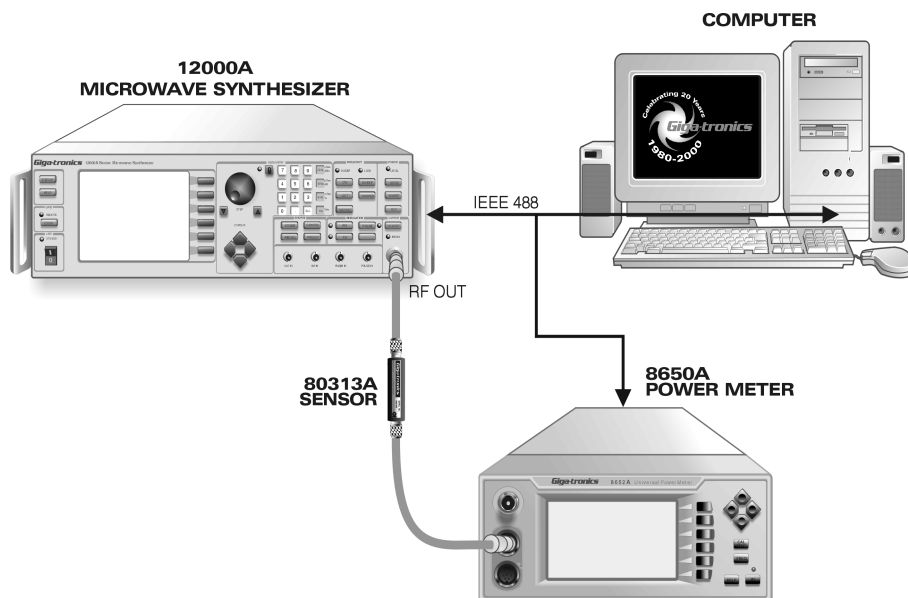
Figure 3-3: Amplitude Modulation Calibration Connection

1. Connect the UUT and computer to the IEEE 488 bus. The UUT should be at address 6 (the default). Connect the DC source as prompted.
2. If the 12000A has not been previously warmed up, allow 30 minutes of warm-up. When the 'Fixed Frequency' screen displays, press the **RF On** button.
3. Start the Calibration Control Program as described in the addendum to this section.
4. Click '**Read Parameters**'. This will interrogate the 12000A and fill in the data on the screen.
5. In the Characterize section, click on the 'AM Calibration' box.
6. The first step requests a zero volts input to the UUT AM connector. Simply leave the input open as there is an internal 600Ω resistor to ground. This test calibrates any zero offset errors. Since AM is DC coupled, any DC component (or zero error) will result in a level shift. Press 'Continue' when ready.

When the prompt requests a 1.0 volt DC input, connect the DC source to the AM input connector and monitor the AM input connector with the voltmeter. Set the DC source to 1.00 volts ± 0.005 volts. It may be helpful to put a resistor of about 6000 ohms in series with the source and the AM input. This will make setting the DC source less critical as it provides a 10:1 divider. Be sure to measure the voltage at the AM input connector with everything connected. This test calibrates the 'full scale' of the AM. Press 'Continue' when ready.

When the prompt requests a 6.0 volt DC input, connect the DC source to the AM input connector and monitor the AM input connector with the voltmeter. Set the DC source to 6.00 volts ± 0.03 volts. Be sure to measure the voltage at the AM input connector with everything connected. This test calibrates the 'full scale' of the Scan Modulation. Press 'Continue' when ready.

3.5.2 Scan Modulation Calibration



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Figure 3-4: Scan Modulation Calibration Connection

Connect the sensor to the meter calibrator (use the 'N' to 'K' adapter) and allow at least 15 minutes for the sensor and meter to reach thermal equilibrium. Then perform a sensor calibration.

Now connect the equipment as shown above. The 80313A sensor connects to the 12000A RF out connector. If the 12000A has a type 'N' connector, use the 'N' to 'K' adapter. The 12000A should have its IEEE address at 6 (the default). The power meter should be at address 10.

If the 12000A has not been previously warmed up, allow 30 minutes of warm-up. When the 'Fixed Frequency' screen displays, press the **RF On** button.

Start the Calibration Control Program as described in the addendum to this section.

Click '**Read Parameters**'. This will interrogate the 12000A and fill in the data on the screen.

- In the Characterize section, click on the 'Modulator (Scan)' box. The purpose of this test is to build a table of correction factors at about 35 frequencies. These values, when applied during Scan Modulation operation, create a linear change in the output level (in dB) as the input voltage is varied from 0 to 6 volts. Scan Modulation is run open loop once the selected CW output level has been set. The correction factors are interpolated for frequencies between the calibration points. This routine will take three to four hours.

Theory of Operation

4.1 Model 12000 Theory of Operation

4.1.1 Overall System description

The Model 12000A is designed using a modular architecture where each basic system functional block is contained on a printed circuit or microwave module. DC power for the instrument is provided by a commercial switching power supply. This supply provides regulated voltages of +6, -6, +12 and -12 volts. The supply is filtered to reduce switching transients and routed to the A4 Distribution PC assembly. This board provides fuse protection, routing and turn-on timing for the supplies to the various other assemblies in the instrument. The A4 board also supplies switching and conditioning for the control lines to the various microwave modules, the step attenuator and Option 20 (High Power). The reference frequency for the instrument, 10 MHz, is supplied by the A15 Time Base PC assembly. The A11 CPU PC assembly supplies all the necessary data processing and control for the instrument. Its inputs include the IEEE 488 bus, the RS232 serial port and the front panel. It controls most of the other instrument PC assemblies via a peripheral data bus. The A11 outputs include many of the rear panel BNC connectors and the display.

Frequency synthesis and frequency modulation are controlled by the A1 Synthesizer PC assembly. This board, in conjunction with the 4-8 GHz YIG oscillator, supplies signals from 1 to 8 GHz. The output from A1 is routed to the A6 and A8 microwave assemblies. The A6 assembly contains the amplifiers, amplitude control elements and harmonic filters for the 2-20 GHz frequency range. The A8 assembly contains the same elements for the .01-2 GHz portion of the output range. Microwave module A7 houses the multipliers and filters to produce 8-20 GHz. Its output is routed to A6 for amplification and level control. The output of A6 is optionally routed through the step attenuator. Control of the amplitude functions (leveling and amplitude modulation) is provided by the A3 ALC PC assembly. This board receives level detector signals from A6 and A8 and returns modulator control signals.

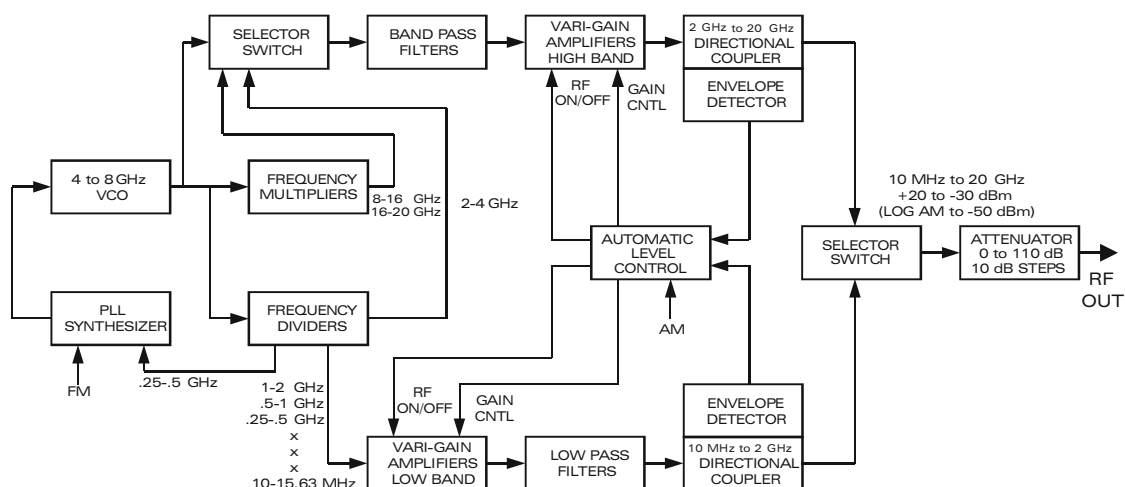


Figure 4-1: Overall Block Diagram

4.2 Power Supply Subsystem (A9)

The Power Supply Assembly consists of two separate power supplies that will accept inputs of 85 to 264 VAC from 47 to 63 Hz:

Standby +12v: Unswitched supply that is operational whenever the AC line cord is plugged in.

Main Supply: Switched Supply that is controlled by the front panel power switch with outputs of +6v, -6v, +12v, and -12v.

The standby power supply is used to provide continuous voltage to the time base oscillator and the YIG heater when the instrument is turned off. When the instrument is turned on, a diode steering network on the A4 assembly switches both the time base and the YIG heater to the main supply. The standby supply is then used to run the cooling fan.

4.3 Power Distribution Subsystem (A4)

The A4 Distribution assembly is used to condition and distribute the main power supply voltages and various locally generated voltages to the other assemblies. In addition, it provides control for the A5/A6/A7 modules, the fan, the step attenuator and the high power option.

4.3.1 Electrical Operation/Circuit Description

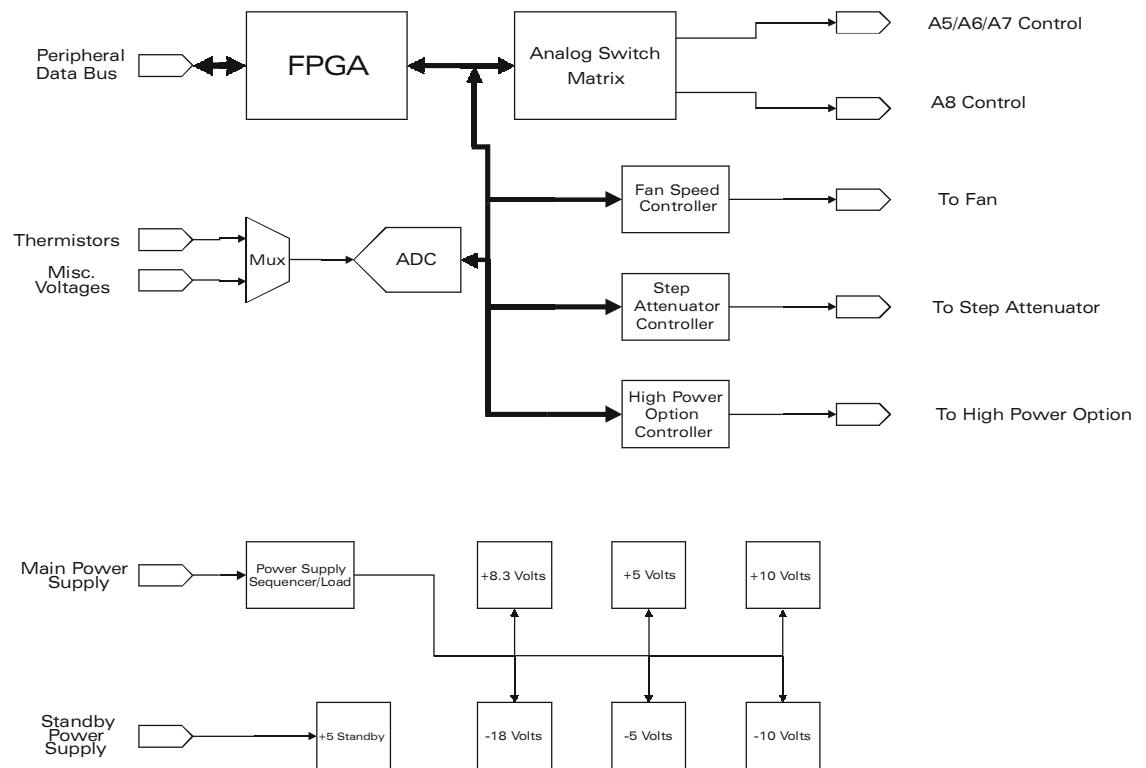


Figure 4-2: A4 Distribution Block Diagram

FPGA Interface

The instrument Peripheral Data Bus provides data from the CPU to the on board FPGA, U101. This device has its program code stored in a fuse-programmable memory chip, U102. The code is loaded into the FPGA at power up. The outputs from the FPGA are used to control all the functions represented on this board.

A5/A6/A7 Control

Control signals from the FPGA are used to drive a series of analog switches (U210-208). These switches send either a positive or a negative power supply voltage to the module interface connector, P201. The voltages are used to bias the various PIN diode switches in the microwave modules and thus select filters and other operational characteristics.

A8 Control

Other outputs from the FPGA are routed directly to the A8 microwave module via connector P102. These logic level signals are translated into appropriate analog signals on the A8 assembly for filter and other switching functions.

Fan Speed Control

IC U302 and its associated circuitry are used to provide control of the speed of the main cooling fan. Thermistor RT301 senses the ambient temperature in the instrument and U302 produces a pulse width modulated signal to control FET Q301 and thus the fan itself. The circuit is set up to run the fan at a minimum speed regardless of low temperature. As the temperature increases above the minimum set point, the fan speed rises proportionally.

Analog to Digital Converter

A multi-input ADC (U301) is provided on this assembly to monitor various voltages and send the information back to the CPU. Inputs are provided to monitor the temperature of each of the microwave modules that has a leveling detector. This data is then used for temperature compensation of the RF level. The timebase VCXO control voltage is monitored to allow calibration and determine if an external source is connected. Monitor lines from the step attenuator and high power options are used to determine the presence of these items.

Step Attenuator Option Control

The optional step attenuator is controlled using driver U304, inverters U303 and transistor Q302. Logic signals from the FPGA are used to control each of the four cells in the attenuator. The cells have values of 10, 20, 40 & 40 dB. Each of the four cells has both an 'on' and an 'off' control line, thus the need for eight drivers. The attenuator has a mechanical device which latches the actuators so the control voltage only supplies current for a few milliseconds at each transition. The attenuator is specially built to have one of the normally unused connector pins tied to ground. This line is monitored to determine the presence of the attenuator.

High Power Option Control

The optional high power amplifier assembly is also controlled from the A4 assembly. Q304 and Q303 provide control for the main power to the assembly. U305 and Q305 are used to select either the .01-2 GHz range or the 2-20 GHz range. Two pin diode drive lines (+5 or -18 volts) are also supplied via U305.

Standby Power Supply

To be able to keep the heaters on the timebase oscillator and the YIG oscillator operating with the instrument turned off, a separate standby power supply is used. This supply produces +12 volts. The steering diodes, CR418, CR419, and C420, ensure that the YIG heater and timebase are driven off the quieter +12V supply during operation. When the unit is in Standby mode, these diodes provide the +12SB voltage. A voltage regulator composed of U405, U406, Q407, and Q408 is used to produce the +5 volts needed by the timebase oscillator. This supply needs to be very low noise, thus the discrete regulator. R432 is used to reduce dissipation in the regulator pass transistor. A voltage monitor (to the ADC) allows determining when the oven is at operating temperature.

Power Supply Sequencing

U401, Q404, Q405 and the other associated circuitry are used to insure that the +12 and +6 power supplies do not come up prior to the negative supplies. A delay is provided by R417 and C402. The power fail signal from the power supply is used to shut off the positive supplies first.

System Power Supplies

Although many of the other assemblies in the instrument produce power supply voltages from the four primary supplies, the A4 assembly does produce a number of voltages.

- The +8.3 volt supply is used by the A6 module for amplifier power
- The –18 volt supply is used to switch PIN diodes on A6
- The +5 volt supply is used for logic power and PIN diode switching on A7/A7
- The –5 volt supply is used for PIN diode switching on A7
- The +/-10 volt supplies are used by the CPU board as well as A5/A6/A7/A8

Each of these supplies is produced by a ‘three terminal’ regulator. The –18 volts is regulated down from a +20 volt switching type boost supply (U410-412). Three devices are used to supply the needed current.

A series of multi-pin connectors distributes the four primary power supply voltages, each of which is fuse protected. A series of green LED indicators signals that each of the primary supplies (and the standby supply) is active. A series of red LED indicators, each connected across one of the fuses, signals that the corresponding fuse has been blown.

4.4 CPU Subsystem (A11)

The CPU board is the main control element within the instrument. Following is a brief list of the resources and functions that the board provides.

Memory Resources

- 2 M of 0 wait state SRAM
- 1 M of Flash memory
- 1 M of battery backed SRAM, expandable by memory expansion board

Next Step Sequencer – provides high-speed sequencing of signals used to change frequencies or power levels.

Peripheral Bus Interface – An 8 bit parallel interface to all other modules in the GT12000A.

Video Controller – Provides interface to a 320 x 240 pixel LCD display on the front panel.

Front Panel Interface – Provides keyboard, LED, Knob, and Piezo Buzzer interfaces.

GPIB – Provides a GPIB interface for the rear panel.

Rear Panel I/O – Provides RS232 interface, Blank / Mark BNC, Stop Sweep BNC, Lock/Level BNC, Trigger In, Trigger Out.

Reset Circuitry

The reset signal for the CPU is generated when the +5V supply drops below 4.65 volts. The main power supply generates a power fail signal which provides at least 5mS warning before the output goes out of regulation after AC power is turned off.

Serial Bus

The LCD contrast, Front Panel LEDs, calibration Trim-DACs on the Time Base board, and an ADC on the Distribution board are all controlled with a serial data bus. Discrete I/O pins from the CPU and one of the I/O ports are used for this bus. The pins are controlled by software to shift data serially into and out of devices. The serial bus is connected to the Distribution Board via P701. Chip select outputs on the CPU enable the LCD contrast and Front Panel LED serial ports. Chip selects for the calibration Trim-DACs and Distribution Board ADC are controlled over the Peripheral Bus by writing values to registers on the Distribution Board.

FLASH Memory

4 – 512 K x 16 word (2 Megabyte) parts provide non-volatile storage for firmware.

Jumper JP201 along with Q203 and associated components allows the FLASH boot block to be programmed. If 12V is provided on the RESET pin, the boot block protection is temporarily disabled and the boot block can be erased and reprogrammed.

NVRAM + Expansion

2 - 512 k x 8 Static RAMs (1 Megabyte) are used to hold the instrument configuration data, settings, user data, and list mode settings when power is removed. A memory expansion connector, P202 allows up to 4 more devices to be added for a total of 3 Megabytes of NVRAM storage. A lithium battery provides backup power.

FPGA

A Field Programmable Logic Array provides the following functions:

Next Step Sequencer –Used to coordinate frequency and power level changes.

Peripheral Bus Sequencer – Controls the transfer of information over the P. Bus.

Front Panel Interface – Provides an interface to the Keyboard, Knob, and Piezo Buzzer.

Peripheral Bus Interface

The Peripheral Bus is used to communicate with other assemblies in the instrument such as the Distribution Board, the Synthesizer, and the ALC. The Address and Data signals are multiplexed onto a single 8-bit bus whose transfer rate is limited to 1 MHz to reduce bus generated EMI. EMI reduction is accomplished by slowing down the signal edges with series resistors and capacitors.

Front Panel Interface

Logic for interfacing to the keyboard, optical encoder, and piezoelectric buzzer is contained in the FPGA. Front Panel indicator LEDs are driven serially by the CPU.

Video Controller

A Graphics Controller and 32 K x 16 SRAM provides a complete video controller to drive a 320 x 240 pixel LCD display. A clock frequency of 6.25 MHz gives a display refresh rate of about 74 Hz.

LCD Bias and Contrast Supply

U507 and associated circuitry provide a –22V bias supply for the LCD panel.

LCD contrast is adjusted by U506. The serial data bus controls U506.

GPIO and RS232 Interfaces

A National Instruments NAT9914 provides all of the control logic for the GPIO interface. A 75ALS160 and 75ALS162 function as GPIO bus transceivers. The GPIO controller shares the CPU's second DMA channel with the CPU's serial port and the I/O Expansion Board. The CPU has two integrated serial ports. A MAX213 translates TTL level signals from both ports to RS232 voltage levels. The device contains built in voltage doublers to translate +5V into levels suitable for RS232.

External Rear-Panel Connections

There are several BNC connections on the rear panel that are controlled by the CPU :

Trigger In, Trigger Out, Lock /Level Out, Stop Sweep I/O (a bi-directional signal) and Blank / Marker. This output is at +5V when MARK/BLANK_HIGH is at +5V, -5V when MARK/BLANK_LOW is at +5V, or 0V out when both inputs are at 0V.

I/O Expansion Connector – P703

This connector provides address, data, and control signals for an additional I/O port

Power Supplies

Linear voltage regulators convert +6 volts down to +5 V and +3.3 V.

4.5 Front Panel Subsystem (A10)

The A10 Assembly accepts outputs from the A11 (CPU) Assy. and sends the information to a 320 X 240 dot LCD display, fourteen LEDs, and a piezo buzzer. The contact information from the 50 pushbuttons and the optical encoder is sent to the A11 (CPU) Assembly.

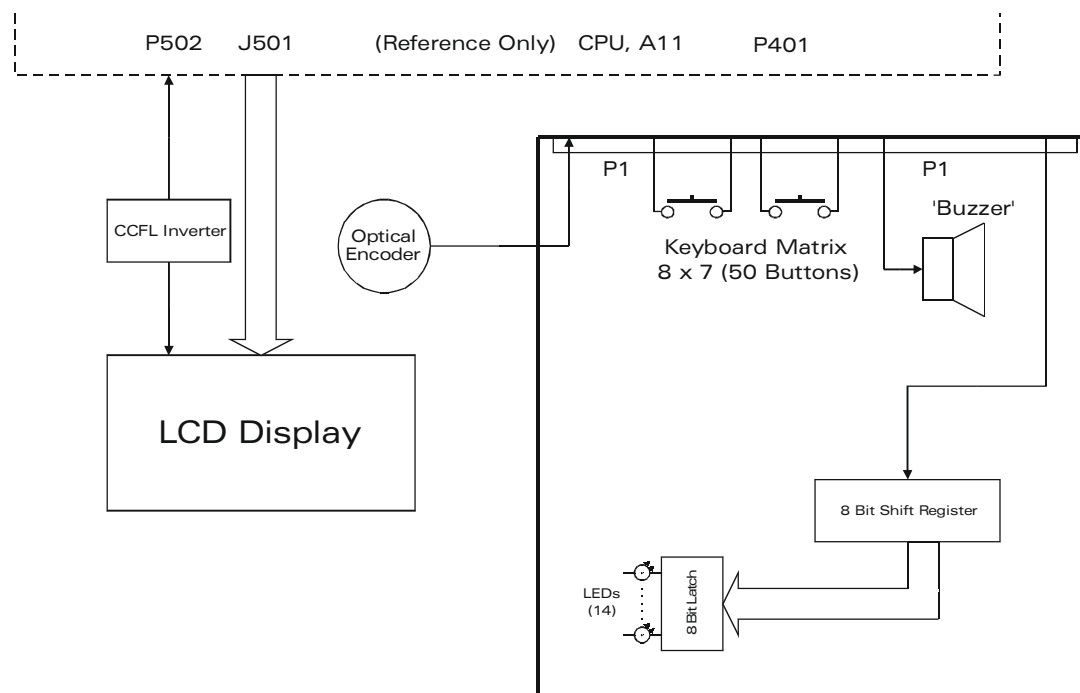


Figure 4-3: A10 Block Diagram

This assembly is functionally divided into six blocks. Three of the blocks are physically on the A10 PCA. The other three blocks are assemblies that are attached to it. Logic for interfacing to the keyboard, optical encoder, and piezoelectric buzzer is contained in the FPGA on A11 (CPU) Assembly.

Keyboard matrix

There are no active parts on this portion of the assembly, only switch contacts. Debounce and decoding are done in software on A11 (CPU). The row and column information is sent to A11 (CPU) via connector P1. The keyboard is an 8*7 switch matrix of 50 pushbuttons. The row outputs are configured as open collector outputs. Normally, they are all driven low at the same time. When a button is depressed, the low is transferred to one of the column inputs and the FPGA interrupts the CPU. The CPU then scans each keyboard row to determine which button was pressed. Continuous scanning of the keyboard is avoided to reduce EMI.

Piezo Buzzer

The buzzer interfaces with A11 (CPU) via P1. The piezo buzzer interface can produce a continuous 2.5 kHz tone, a 5 kHz tone, or a single click. The CPU controls tone duration by turning the tone on or off. The click is a single 100uS pulse applied to the piezo buzzer. Piezo volume can be set to 8 different levels. Level 0 is off, and level 7 is the highest volume level.

LEDs

Serial data from A11 (CPU) via P1 enters two 8-bit shift registers where it is converted to parallel data that is routed to two 8-bit Latches. The latches store the LED information and also drive the fourteen front panel LEDs.

Inverter Supply

This supply is attached to the A10 Assembly. The supply accepts +5V from the A11 (CPU) Assembly and outputs 230VAC to the LCD assembly for backlight illumination.

LCD Module

The assembly is attached to the A10 Assy. LCD data and contrast signals come from the A11 (CPU) Assembly. The display is mounted to the Signal Generator's front panel, and connected via a ribbon cable to A11 (CPU) J501. The ribbon cable carries all of the signals and power for the display.

Optical Encoder

The encoder mounts to the front panel and is connected to the A10 Assembly with a five-pin cable. The optical encoder is driven by a knob on the front panel and has 64 counts per revolution. Turning the optical encoder knob rapidly, about 3 revolutions per second, produces about 200 counts per second.



Regardless of whether the operating frequency is derived from the internal crystal oscillator module or an external source, it is the internal module that actually feeds 10 MHz to the A15 outputs. The oscillator feeds three high current buffers. Two outputs of are paralleled and feed J8; the remaining one feeds the inputs of the other eight buffers which feed the remaining coaxial output connectors.

When there is no external frequency reference signal present, the oscillator tuning control voltage is maintained by the CPU at a level determined at the last calibration. The CPU can constantly read the control voltage and adjust it by controlling a digital potentiometer.

Whenever an External Frequency Reference signal is present an envelope detector senses the signal and provides an output to switch control of the VCXO to a phase lock loop. This PLL locks the VCXO to the external source with a very slow loop to filter most of the noise from the external signal. Divider U2A allows the PLL to accept a 5 MHz external source in addition to a 10 MHz one.

4.6.1 Synthesizer Subsystem (A1)

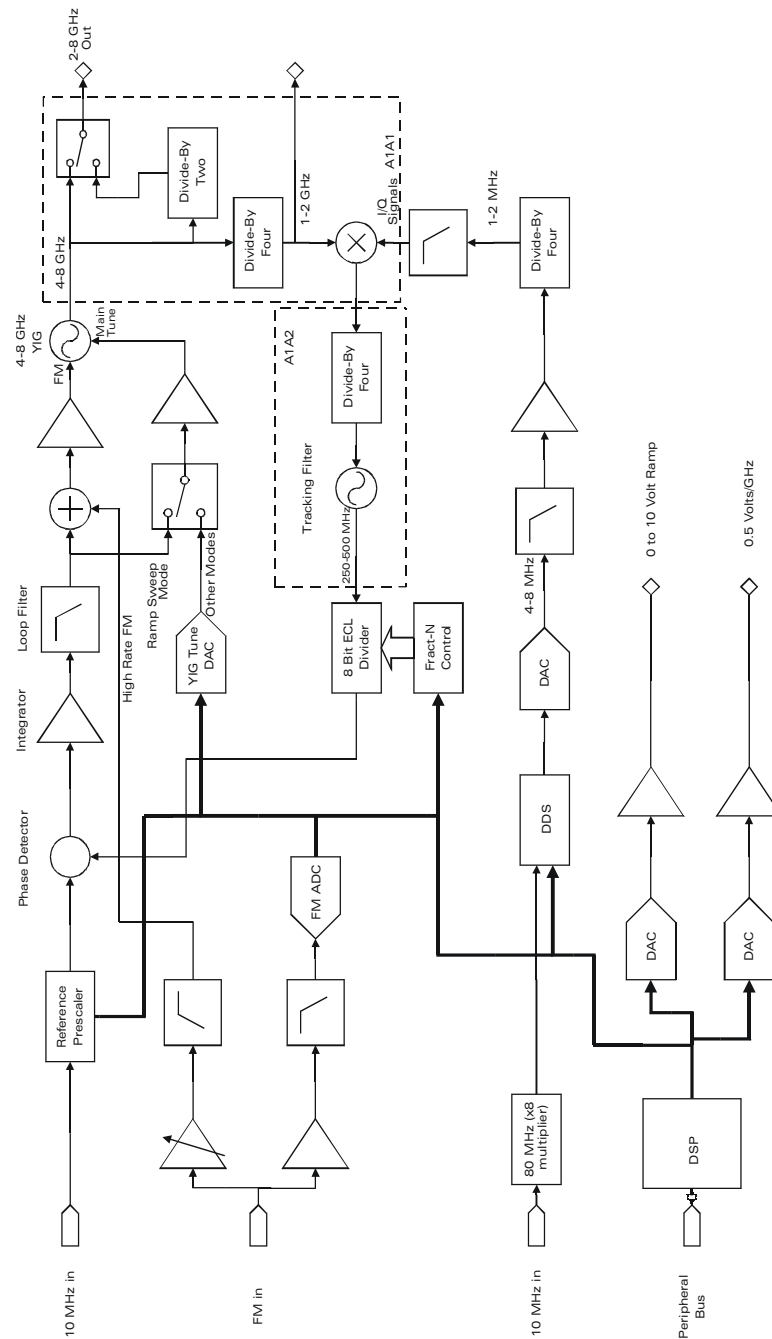


Figure 4-5: A1 Synthesizer Block Diagram

The A1 PC Assembly is used to generate the basic synthesized signal for the instrument. All elements of this function other than the YIG oscillator and the YIG driver FET are contained on the board or on the attached A1A1 and A1A2 assemblies. The assembly provides all the frequencies from 1 to 8 GHz.

The synthesizer may be logically divided into a number of sub-blocks. These are: (1) The primary synthesis loop (2) The high resolution DDS (3) The YIG oscillator main tune coil driver (4) The frequency modulation system and (5) The control system.

Primary Synthesis Loop

The primary synthesis loop consists of the Phase Detector, Integrator, Loop Amplifier, YIG Oscillator, A1A1/A1A2, and the Divide-by-N.

The 10 MHz reference input for the phase detector is produced on the A15 Timebase board and is an isolated output to avoid adding any noise to the signal. On the A1 assembly, the 10 MHz is normally routed directly to the phase detector. A divide-by-four pre-scale is used when in the wide FM mode. The other input to the phase detector comes from the output of U510, a programmable 8 bit counter. The preset inputs of this counter are controlled by FPGA U508. The primary purpose for this FPGA is to do the necessary tasks to implement the "Fractional-N" required to obtain 4 MHz resolution in the main loop.

The input to the 8 bit counter comes from the output of the A1A2 tracking filter. This frequency varies from 250 to 500 MHz over the 4-8 GHz range if the YIG oscillator. The counter output drives the 'variable' input of the phase detector (flip-flops U513 and gate U518). Its two outputs go to the integrator.

There are actually three separate integrators used. The first, a 'double integrator' (U601A & U601B) is used in the 'CW' mode (i.e. no FM and not in Ramp Sweep). The extra integrator stage provides additional gain for noise suppression. The second integrator (U602) is used for the wideband FM mode. The remaining integrator (U603) is used for Ramp Sweep. This mode uses the main tuning coil of the YIG oscillator rather than the FM coil. Since the sensitivity and response characteristics are considerably different, a separate integrator is needed.

Amplifier U606 provides a low impedance drive for the loop low pass filter. This filter is included primarily to suppress the 'delete rate' spur of 250 kHz (produced by the Fractional-N). Following the filter is gain control amplifier U608. The gain of the loop will vary as the 'N' number is changed. In this case, a 2:1 change will occur from 4 to 8 GHz. To both maintain stable loop operation and also to allow the FM to work properly, the gain of the loop must be increased as the 'N' number increases.

The final elements of the primary synthesis loop are filter C742, L703, C743 and the FM coil driver U701. The filter provides additional high frequency attenuation. The FM coil driver is a high current device (about 200 ma output) which drives the YIG oscillator FM coil.

High Resolution DDS

To enable the synthesizer to have 0.1 Hz resolution, a Direct Digital Synthesizer (DDS) is used in conjunction with a SSB mixer in the A1A1. This DDS is programmed by the DSP and produces steps of 0.025 Hz. Due to the divide-by-four prior to the SSB mixer in the A1A1, the DDS output is effectively multiplied by four at the output of the synthesizer.

YIG Oscillator Main Tune Coil Driver

The driver for the YIG main tune coil converts a voltage based 'command' from the control system into a current which tunes the oscillator. The tuning resolution is approximately 60 kHz. The driver also includes the circuitry to switch in the noise reduction capacitor.

A 16 bit DAC (U702), controlled by the DSP, and amplifier U705B provide a voltage proportional to frequency. Amplifier U705A compares the voltage from the DAC to the amplified voltage from the current sense resistor R724. The output of the amplifier is used to control power FET Q703. This FET, in series with the supply voltage to the YIG oscillator main tune coil, effectively sets the current through the coil and thus determines the frequency.

To maintain a fast switching speed, it is necessary to minimize any capacitance across the YIG coil. This, however, results in considerable noise being applied to the oscillator and would degrade the spectral purity of the output signal. To reduce the noise, capacitor C746 is connected across the main tune coil once the instrument has acquired phase lock after a frequency change. The capacitor must be 'pre-charged' to exactly match the voltage across the coil prior to being connected to prevent transients.

 **NOTE:** *There are no adjustments in this circuit. Each time the instrument is powered up a calibration routine is run to determine the proper setting for the DAC to produce a locked condition with the loop control voltage close to zero. Two points are determined, one near 4 GHz and the other near 8 GHz. The computer then uses this information and linearly changes the DAC output proportional to the desired frequency. During instrument operation (in most modes other than sweep) the loop voltage is monitored and the setting of the DAC is changed, one bit at a time to maintain the loop near zero. This change is not noticeable and automatically corrects for any drift or non-linearities.*

Frequency Modulation System

External frequency modulation for the instrument is controlled entirely by this assembly. Since the modulation frequency spans DC to 1 MHz, it is necessary to modulate both 'within the loop' and 'outside the loop'. Modulation inside the loop is accomplished using the DDS, modulation outside the loop is summed directly into the YIG FM coil driver.

The signal for the 'Inside the Loop' portion of the FM goes through active filter U312, a fixed low-pass filter and the high speed ADC. The digitized signal is sent to the DSP which uses it to reprogram the frequency setting of the DDS at a 1 MHz rate, thus frequency modulating the DDS output. Since the control is wholly digital and the input is DC coupled, true DCFM is possible with full synthesizer accuracy.

The signal for the 'Outside the Loop' portion of the modulation (effectively everything above 15 kHz) passes through a high pass filter to remove the DC component. The signal for this path has its level adjusted to match the deviation of the inside the loop portion by DAC U302 and analog multiplier U303. Additional gain selection (primarily for input sensitivity setting) is provided by a resistor network, switch U304, and amplifier U305. The output of U305 goes to the YIG FM coil driver.

Due to the phase shift caused by both the primary loop and the tracking filter loop, it is necessary to provide additional compensation to maintain the flatness specification of the deviation. Amplifiers U318 and U320 comprise active filters to produce the required correction. The correction signal amplitude is adjusted using DAC POT U319. During narrow FM operation, switch U604 connects the correction signal directly into the phase detector.

Control System

The various functions and operations of the Synthesizer are controlled by various logic devices. Commands from the host CPU are sent to the Synthesizer via the Peripheral Data Bus. A DSP, U104, and a CPLD, U105, decode these commands and route them to the appropriate destinations.

Two analog output signals are generated on the Synthesizer board. These are the 10 volt ramp and the 0.5 volt/GHz output. The 10 volt ramp is a signal used during sweep modes and goes from zero volts at the start of a sweep to 10 volts at the end of the sweep. The 0.5 volt/GHz signal is always present and is proportional to the operating frequency.

A multiple input Analog to Digital converter (U710) is monitored by the control system to provide information on various voltage levels. These include the PLL voltages for both the primary and tracking filter loops, various FM system voltages, and the YIG driver. The readings are used for the calibration and automatic adjustment functions.

Series 12000A Microwave Synthesizers

Because the synthesizer is sensitive to noise on the power supplies it uses, on board regulators are provided. The majority of these consist of an op-amp and power transistor rather than a packaged regulator. This is done to provide the lowest noise. A precision reference, U807, supplies 5 volts to the regulators. U810 is a switching boost type regulator used to provide 20 volts for the YIG driver and the tracking filter VCO drive.

The Ramp Sweep mode of operation uses a different method to achieve phase lock. Rather than using the YIG driver to coarse tune the YIG and the FM coil to close the loop, the YIG DAC is not used and the loop voltage is fed to the main coil via the remaining driver circuitry. This permits ramp sweep to operate by stepping the frequency in very small (sub-hertz) steps at a high rate of speed.

4.7 Microwave Signal Conditioning Subsystem (A6/A7)

A6 Output Module

The output module (A6) is a wide-band component (2-20 GHz) that provides most of the processing functions of the microwave signal such as: amplification, harmonic filtering, amplitude modulation, and pulse modulation. It can accept the .01-2 GHz signal from the optional Digital Down Converter (A8) to provide .01 to 20+ GHz coverage from a single test port and features a built-in 2-20 GHz directional detector as part of the ALC function.

PIN Diode Pulse Modulator

Located at the input of the module (J1), this component provides high speed amplitude modulation of the 2-8 GHz signal delivered from the synthesizer module. Pulse modulating the 2-8 GHz signal provides the added benefit that subsequently multiplied signals (8-20 GHz through A7, and 20-40 GHz through A5) can also be pulse modulated with no added hardware.

Gain Blocks A1-A4

The gain blocks are GaAs MMIC with dual-gate FET cells. The gain of A1 and A2 are varied together for ALC and AM application, A3s and A4s gain control input provides scan modulation.

Switched-Low Pass Filter

The 2-20 GHz spectrum is redirected into 5 sub-bands (2-3.2, 3.2-5.1, 5.1-8, and 8-20 GHz) with low-pass filters to remove harmonics. An additional switch arm on the output side can also receive the low-band signal (.01-2 GHz) from the optional Digital Down Converter (A8).

Directional Detector

The directional detector consists of a multi-section microstrip coupler with dielectric overlay compensation, built-in termination and a single-diode broadband detector at the coupled port.

4.7.1 A7 Multiplier

The function of module A7 is to produce the 8-20 GHz signal from the 4-8 GHz received from A6, and to remove the spurious products of frequency multiplication by band-pass filtering. The 4-8 GHz signal is first multiplied by a frequency doubler (ADA1) to produce 8-16 GHz. The output is then split into four bands by a SP4T PIN diode switch; the first three are band-pass filtered to produce the following frequencies: 8-10.1 GHz, 10.1-12.7 GHz, 12.7-16 GHz. The 8-10.1 GHz band is also used to drive the second frequency doubler (ADA2) to produce 16-20.2 GHz. The four frequency bands are filtered to remove the $1/2$ s and $3/2$ s spurious signals and combined by a second SP4T switch.

4.8 Interface Assembly (A17)

This printed circuit assembly is used to connect microwave assemblies A6 (2-20 GHz Output Module) and A7 (Multiplier Module) to the rest of the system. The board provides signal conditioning and routing for both the detector outputs and some of the modulator inputs. Connector P1 delivers power and PIN diode switching signals to both A7 and A6. PIN diode signals (for switch filters) pass through resistors R8-R20 before connecting A6 and A7.

There are two amplifier channels used as detector buffers. One, for CW operation, provides low noise, low drift gain. The other, for pulse operation features fast rise time. The outputs feed the ALC assembly.

4.9 Down Converter (A8)

The Digital Down Converter module accepts signals in the range of 1-2 GHz at 4-8 dBm and outputs signals in the range of .01-2.0 GHz at -25 to +18 dBm. The module also provides pulse modulation, amplitude modulation, harmonic filtering, and signal level detection for automatic level control Functional Block Diagram.

The Down Converter is divided functionally into four major circuit blocks:

The Source Block

This is a chain of programmable frequency prescalers and a SP4T switch-combiner. The prescalers perform frequency division ($n=2, 4, 8, 16, 32, 64, \text{ or } 128$) on the input signal and the SP4T selects the outputs of the various prescalers which is sent to the Amplifier and Modulator Block. To prevent the generation of the sub-harmonics of the desired signal that are impossible to remove later, unused lower-order prescalers are turned off.

The Amplifier and Modulator Block

This section provides signal amplification, attenuation (modulators), and pulse modulation (ON/OFF) for the full output frequency range of .01 – 2.0 GHz. The amplifiers and modulators are organized in a distributed fashion to minimize the interaction over the frequency range.

The Switch-Filter Block

The incoming signals from the Amplifier/Modulator are directed into fifteen contiguous frequency bands to reduce harmonics. To facilitate signal-blanking and band-switching from the system standpoint, each filter's operating bandwidth is exactly one-half octave wide and a sub-multiple of the original input frequency range (1.0-1.414 GHz, and 1.414-2.0 GHz). The switch-filter matrix is arranged such that the signals that pass through the six lowest-frequency filter bands will be pre-filtered by a filter 3-octaves higher in frequency. The directional coupler and detector located at the output samples and detects the output signal level for ALC and AM purposes.

The Control Logic Block

This portion provides proper drivers to interface between the Down Converter and the Distribution module (PIN diode switch drivers) and between the Down Converter and the ALC module (PM and AM drivers and detector amplifier).

System Interface

R.F. input is supplied by the A1-A1 synthesizer front end and R.F. is output to the A6 output module. The module receives regulated power supply voltages and TTL commands from the Distribution Module (A4) via a multi-pin connector.

4.10 Automatic Level Control (A3)

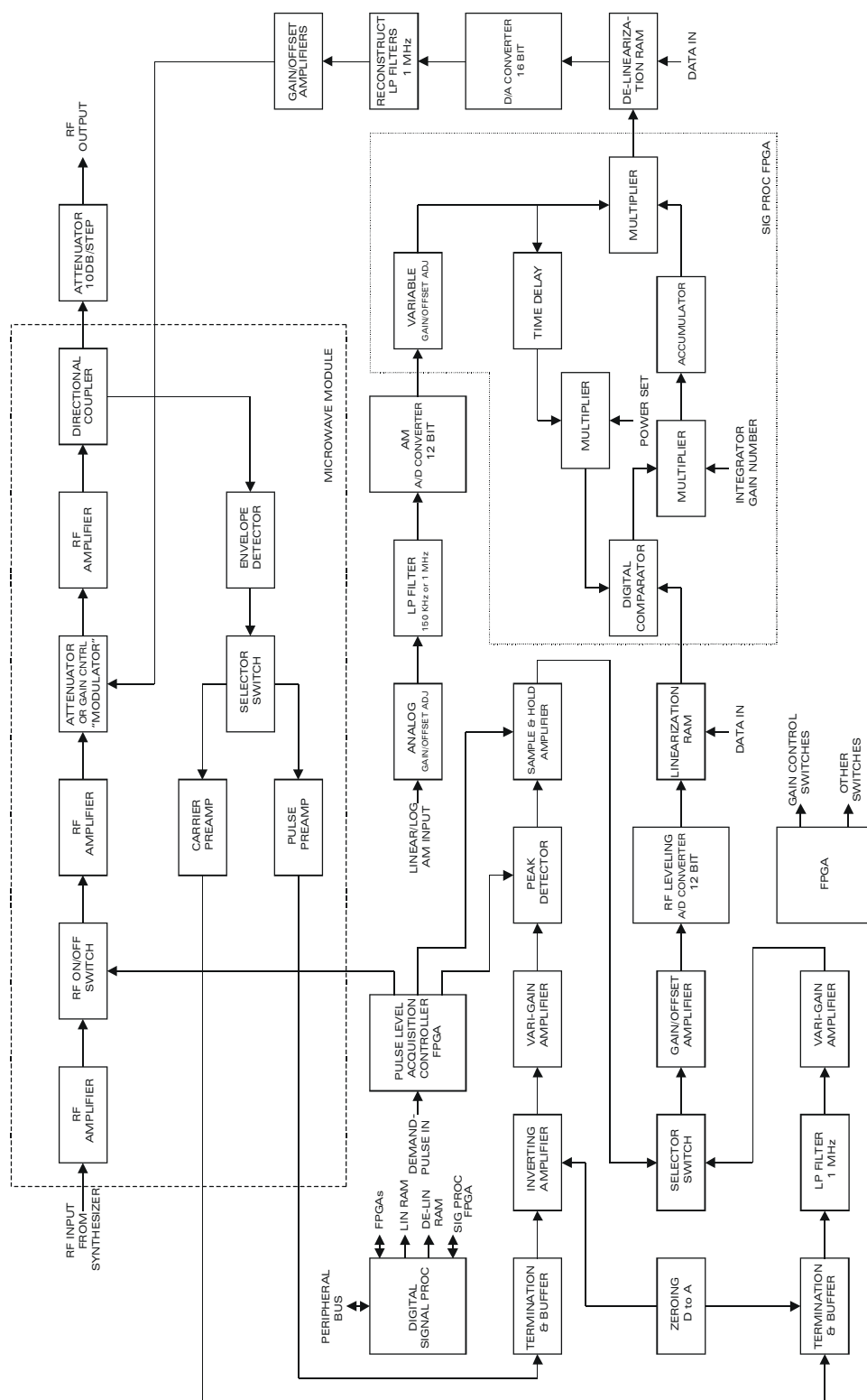
The Automatic Level Control (ALC) board (A3) contains a feedback control system that maintains the RF output amplitude in accordance with the desired value. It also provides linear Amplitude Modulation (AM), Logarithmic Amplitude Modulation (“Scan”), and Pulse (square wave) Modulation (PM), using whatever arbitrary modulation waveform or timing it receives from the modulation signal sources outside of or within the 12000A chassis.

Closed loop power control of an RF amplifier subsystem can be maintained by the ALC from +20 dBm to –20 dBm. Open loop power control (used for Log AM) can range from +20 dBm to –50 dBm. When the optional 110 dB, automatically controlled 10 dB step attenuator is installed, the range is expanded down to –130 dBm. This electromechanical attenuator permits the RF amplifier subsystem to operate between 0 dBm and +10 dBm for all 12000A output CW levels and AM carrier levels, (except above +10 dBm). Log AM fiduciary levels range between +5 and +15 dBm.

Under normal closed loop critically damped operation, leveling time is about 100 μ seconds. By jamming measured, saved, and updated final drive level requirements as a function of 12000A output power into the integrator accumulator just before the leveling loop is closed, leveling time can be reduced to a few microseconds.

The 12000A contains up to three RF amplifier subsystems—for 10 MHz to 2 GHz (A8), for 2 GHz to 20 GHz (A6/A7/A17), and for 20 GHz to 40 GHz (A5). Each of these subsystems contains analog RF gain control elements that the ALC uses as the final drive to control output power level. At the output of each of these subsystems is a directional coupler, diode envelope detector, and a set of video preamplifiers to provide the ALC with a monotonic DC voltage scale of instantaneous RF envelope output power. During the automatic characterization procedure (see Section 3.4), a record of DC voltage vs. RF output power (actually peak RF voltage) at various frequencies is obtained.

The following conceptual block diagram (Figure 4-6) shows the above connections between a typical 12000A RF amplifier subsystem (“microwave module”) and the ALC board. Also shown is the ALC board controlling the RF on/off switch, which is also used as the final drive for Pulse Modulation.



4.10.1 General Architecture

Owing to the time it takes for a signal to propagate completely around the control loop (especially including through the gain control elements and RF amplifiers), the servo loop bandwidth is limited to about 10 KHz. However (for reasons explained below), all stages in the main loop are flat from DC up to almost 1 MHz.

The ALC servo element is a high speed, digital hardware-based integrator contained within a Field Programmable Gate Array ("Sig Proc FPGA"). Also contained in this FPGA is gain and offset adjustment of the digitized AM input signal and the means to apply this signal to both the input and output of the integrator. The integrator is broken down into a comparator, multiplier, and accumulator. Multiplying the difference between the desired RF voltage ("Power Set") and instantaneous RF voltage by a selected "integrator gain number" allows the speed of accumulation to be controlled, thus allowing the entire control loop gain to be set for the quickest stable operation.

Preceding the integrator is the 12-bit RF Leveling A/D and lookup table ("Linearization RAM") that allows it to see a linear RF voltage scale, despite the nonlinear transfer characteristics of the diode envelope detectors in the RF amplifier subsystems. Preceding the A/D are two selectable gain controlled amplifier subsystems—one each for CW and Pulse operation. Their principal use is to convert the widely variable detected and pre-amplified signals to the +1 Volt to +4 Volt scale needed by the A/D.

Following the integrator accumulator and feed-forward Linear AM modulator multiplier (inside the Sig Proc FPGA) is another lookup table. This "De-linearization" RAM permits linear changes of the integrator output to result in linear changes of 12000A RF output voltage, despite the grossly nonlinear (mainly logarithmic) transfer characteristics of the gain control elements located in the various RF amplifier subsystems.

The digital control signal is now converted to an analog signal and then gain-and-offset adjusted in separate selectable circuits to accommodate the peculiar gain control curves of each of the three RF amplifier subsystems. The RF output level vs D/A converter count value at various frequencies is measured and stored during the characterization process.

4.10.2 CW Operation

The selector switch in the particular RF amplifier subsystem selects the "carrier" preamplifier. (This preamplifier is also used for Linear AM and calibration of Logarithmic AM.) This preamplifier is optimized for voltage offset stability and low noise. It includes a 20 K-Ohm termination for the detector to maximize its temperature stability and output level. Its DC to 1 MHz bandwidth is needed only for Linear AM; only DC to 30 KHz is needed for CW.

At the ALC Board input is a switch (not shown) that selects one of the three RF amplifier subsystems or an external detector. The RF leveling A/D converter samples its input data at a 10 MHz rate (but only every other sample is used). The 1 MHz low pass filter prevents aliasing of the higher frequency components.

The DC signal level at the ALC Board input varies from several Volts to several millivolts as the 12000A RF output varies from +20 dBm to -20 dBm. In order to maintain an adequate count value per dB set point resolution for small signals without overloading the A/D converter when the signal is large, the gain is adjusted in seven steps over a 250:1 range by the Variable Gain amplifier. The Gain/Offset amplifier is used mainly to shift the voltage scale from 0-3 Volts to 1-4 Volts, needed by the A/D converter input.

The buffer amplifier includes insertion of an offset voltage by the Zeroing D/A converter. During each 12000A boot-up process, the correct D/A converter value is determined for each gain setting; so that the zero-signal A/D count level is consistent over time, regardless of long term offset drift in the diode detector/carrier preamplifier or elsewhere.

Inside the Sig Proc FPGA, the feed-forward Linear AM modulator and power set multipliers are locked to multiply by one. The integrator accumulator counts up or down depending upon whether the “Power” Set input level is higher or lower than the instantaneous signal level delivered by the A/D and Linearization RAM. The speed of counting is directly proportional to the magnitude of this disparity and Integrator Gain Number.

4.10.3 Linear AM Operation

Most of the sophistication present in the ALC result from the requirement to deliver accurate carrier level regulation and low distortion, high modulation index (upward and downward) Linear AM at all modulating frequencies between DC and 150 KHz. Three significant architectural features were employed to meet these requirements:

1. The servo control element sees a linear (voltage) control loop in both the feedback and feedforward directions. This is accomplished despite the nonlinear transfer characteristics of the detector and gain control elements by the two lookup tables. Therefore, the instantaneous open loop RF voltage envelope is proportional to the count value entering the integrator comparator, and any error in the RF voltage is proportional to comparator output and thence the rate of accumulator slew. Finally, the instantaneous open loop RF voltage envelope is also proportional to the accumulator count value. These design measures combine to provide for low distortion closed loop Linear AM at all modulation levels and all RF carrier levels.

The basic Linear AM process is similar to that found in other closed loop level control systems. The number representing the desired or demanded RF output voltage feeds the comparator reference input through a multiplier, and the other multiplier input receives the modulating signal input. When this modulating signal is at zero level, its multiplier is unity, causing the envelope output voltage to have its unmodulated, carrier level set value. As the modulating voltage varies from its maximum allowable value to its minimum allowable value, the multiplier input value goes from 2 to 0, and the RF voltage goes from twice the carrier level to zero—so demanded by the comparator reference input.

2. Closed loop modulation control is limited, however, to about 10 KHz, commensurate with the highest speed at which the servo loop can apply small phase margin corrections. In order to handle the full spectrum of modulating frequencies, all modulation spectral content that cannot be handled by the loop bandwidth must be injected (fed forward) after the integrator. In the 12000A, the entire modulating spectrum multiplies the carrier level (digital) value, analogous to classical analog high level AM of a Class C amplifier, wherein the voltage that is proportional to RF output power is multiplied by the modulating voltage. There are no crossover elements (except for the servo loop itself) to separate the portion of the spectrum that can and cannot be controlled by the loop. The composite subsystem amplitude and phase response is completely flat up to 150 KHz; there is no indication of where the modulation is inside or outside the loop. The “Time Delay” allows the feedforward modulation information to go around the loop and reach the integrator comparator at the same time as the feedback component.

3. When the RF signal is modulated at a high level with a 150 KHz sine wave, the waveform at the envelope detector output contains the fundamental and several harmonics up to 750 KHz, principally at 300 KHz and 600 KHz. If only the fundamental is considered (harmonics suppressed), the 150 KHz sine wave will have an average value that depends upon the degree of modulation, causing the carrier level adjustment to become increasingly inaccurate as the modulation index is increased. Therefore, a 1 MHz bandpass is maintained in all analog and digital circuitry at least through Linearization RAM lookup table. Similarly, all circuitry between the De-linearization RAM through the gain control elements must have a 1 MHz bandpass to contain the important harmonics commensurate with an exponentiated 150 KHz sine wave.

Before being fed to the Sig Proc FPGA, the AM-intended signal passes through a gain and offset adjustment that maps a $-1V$ - $+1V$ scale to a $0V$ - $5V$ scale. It then passes through a 150 KHz anti-aliasing filter and the AM (12-bit) A/D converter.

4.10.4 Logarithmic ("Scan") AM Operation

Log AM uses the same 12000A input connector and A/D converter, but the input scale is $0V$ to $6V$ (for 0 to 60 dB reduction from the fiduciary CW set point level), and a 1MHz anti-aliasing filter is needed. The 12000A Scan Menu allows other scales than 10 dB/Volt, and these are obtained by the Variable Gain adjustment block in the Sig Proc FPGA.

Log AM operation is carried out totally open loop (unlike its calibration, which is done closed loop by the CW infrastructure). Open loop operation is needed for two reasons:

1. The speed is too high for the 10 KHz feedback control system; a 50 dB change over a μ second or less is guaranteed.
2. A 60 dB range below the fiduciary level is guaranteed. Owing to the high speed involved, the 10 dB/step electromechanical attenuator is much too slow during operation (but is used to set the fiduciary level). More than 40 dB below the fiduciary level, there is insufficient feedback signal level coming from the detector to operate the servo loop.

Although the Figure shows a single gain control point in the RF amplifier subsystem, there are actually two cascaded gain control points, each controlled separately or in unison by the ALC. Each gain control point has a range of at least 40 dB. Only one of them is used in CW, Linear AM, and Pulse Modulation, while the other is maintained at minimum attenuation. In Log AM, both are needed to obtain the 60 dB or more range.

During factory Log AM (Scan) Characterization (which can be repeated periodically in the field), open loop measurements are made using an external power meter. A D/A converter count vs power output scale is obtained for many frequencies over the 12000A frequency range.

The shape of this scale is stable, but the gain control elements (and other aspects of the RF amplifier subsystem and RF source) offset-drifts with temperature and time. Therefore each time the AM ON switch is actuated, the system first switches briefly to CW, and a closed loop single point calibration is performed at the fiduciary level. This offset calibration is performed each time the 12000A carrier frequency and/or fiduciary power level is changed.

4.10.5 Pulse Modulation (PM) Operation

The RF output level for PM (Square Wave Modulation) is entirely under closed loop control, but there are several differences in the way this control must be effected.

The pulse timing (when the RF output is on or off) is independent of the method used to control the output level. The digital “demand” pulses from the external source or optional internal Modulation Generator directly operate the set of RF on/off switches in the RF amplifier subsystem.

In CW and Linear AM operation, the 12000A is delivering RF at all times; so the feedback signal is automatically always present at the envelope detector, and the RF Leveling A/D converter input. For PM however, a feedback signal is present only while the RF pulse is on, which for very short pulses (such as 50 nSec) can be an extremely short percentage of time. Therefore, special circuitry is needed to capture detected pulse level and hold it a long enough time for the control system to use it and until the next pulse arrives (with its new level information). The PM detected signal also differs from CW and Linear AM in that the narrow pulses and rapid rise time represent a much wider bandwidth than 10 KHz to 1 MHz—at least 20 MHz, which affects both the amplifiers and even the envelope detector itself.

In the respective RF amplifier subsystem, a broadband, higher gain preamplifier is used. Its input terminates the diode detector with only 1 K-Ohm, needed in order for the diode to respond rapidly enough. Such low terminating impedance degrades both the detected signal level and temperature stability.

The ALC board includes a broadband variable gain amplifier and the necessary circuitry to capture the detected pulse amplitude. It is not necessary to determine the detected pulse’s presence directly; as its presence is directly correlated with the demand pulse, albeit with a delay. This delay cannot be controlled in Production with sufficient precision to capture the level in a Sample and Hold circuit by itself; so preceding it is a peak detector, which—unlike the Sample and Hold—requires no control signal to capture the level. (The peak detector control line shown in the Figure is used only to reset it.)

The Pulse Level Acquisition Controller FPGA receives the Demand Pulses and passes them immediately to the RF on/off switches. It uses the timing of these Pulses as well as the A/D converter sample clock to operate the sample and hold circuit and peak detector Reset controls. For all pulses longer than several hundred nanoseconds, the pulse height is re-read every 200 nanoseconds.

Each time the Pulse-Modulation-On switch is operated, or the 12000A frequency or RF output level is changed, before the pulse pattern is admitted, the system is switched briefly to CW operation and the D/A converter count noted. Then the system is switched (back) to the Pulse chain, and its zeroing is adjusted until the same D/A converter count is obtained. Thus, the long-term accuracy of CW is obtained for PM.

4.10.6 Digital Communication, Controls and Calculations

In addition to the signal chain components (A/D, D/A, Sig Proc FPGA, and lookup table RAMs) and Detected Pulse Acquisition Timing FPGA, the following major digital components are present on the ALC Board:

The Digital Signal Processor (DSP, U104) receives demanded level data from the Host CPU. It also receives polynomial coefficients from the CPU and expands them to calculate the lookup tables, which it sends to the Linearization and De-linearization RAMs via the Sign Proc FPGA over the lower 16 lines of its 24 line parallel bus. It coordinates all activities on the board with the help of its intra-board serial bus I/O system. This serial bus services the System and I/O CPLDs, the Detected Pulse Acquisition Control FPGA, and the three auxiliary serial DACs.

The system CPLD (U202) operates all the chip selects. It also operates the twelve switches that control the main D/A converter drive to the various RF amplifier subsystem gain control elements and the Load command for the three serial DACs. The data and timing for these functions come from the serial bus. Finally, along with the DSP, this CPLD is connected directly to the Peripheral Bus; so that it can provide its hardware support—including boot support.

The “I/O” CPLD (U203) contains the latches that operate all the analog switches except for those following the D/A converter, including gain setting, detector source selection, modulation type/source selection, CW/PM selection, and filter selection. It also drives the DSP Reset. The control and data come from the serial bus.

In addition to the servo integrator and signal processing functions, the Sig Proc FPGA serves as the distribution device for all parallel data and address lines used by the Linearization and De-linearization RAMs. It does this in order to intersperse loading new tables in one memory segment at the same time (alternate clock cycles) while using a previously loaded segment for leveling.

All communication between the 12000A Host CPU (A11) and ALC Board is provided by the Peripheral Bus. Dedicated inputs include Read, Write, and Reset controls, Sweep Synchronization, Marker, and Sweep Start Timing, Strobe, and RF ON. Dedicated outputs include Ready to Level, Leveling Complete, and Interrupt Request. There is also a bi-directional 8-bit data bus.

Replaceable Parts

5.1 12000A Replaceable Parts

Table 5-1: 12000A Replaceable Parts List

P/N	Item description
30572	A1 Synthesizer PCA
31288	A1-A1 Synthesizer Front End assembly
31542	A1-A2 Track Filter assembly
30580	A3 ALC PCA
30584	A4 Distribution PCA
30570	A6/.01-20GHz Output module
30577	A7/8-20GHz Multiplier module
30596	A8 Downconverter assembly
31632	A9 Power Supply assembly
30751	A10 keyboard PCA
30755	A11 Main Processor PCA
30913	A15 Time Base PCA
30771	A16 Modulation Generator PCA
31740	A17 Interface PCA
31891	A18 Power Supply Filter PCA
31807	Upper rear mount feet
31917	Lower rear mount feet
30727	Handle
MPBO-02001	Option 26 Attenuator
IMCO-00002	320 x 240 LCD Module
KGRO-15025	1.50" diameter knob with spinner
FSAC-00200	2A SB Fuse, 3AG
HFBI-00014	Mount bail
HFFL-63202	Left front feet
HFFR-63202	Right front feet
BHGO-05000	Fan finger guard
BHSO-05000	Fan screen
BDOO-05012	12VDC 4-5/8" fan
JRAB-00200	SMA Bulkhead connector
JRDF-00004	BNC panel mount connector

Troubleshooting

6.1 12000A Fault Isolation

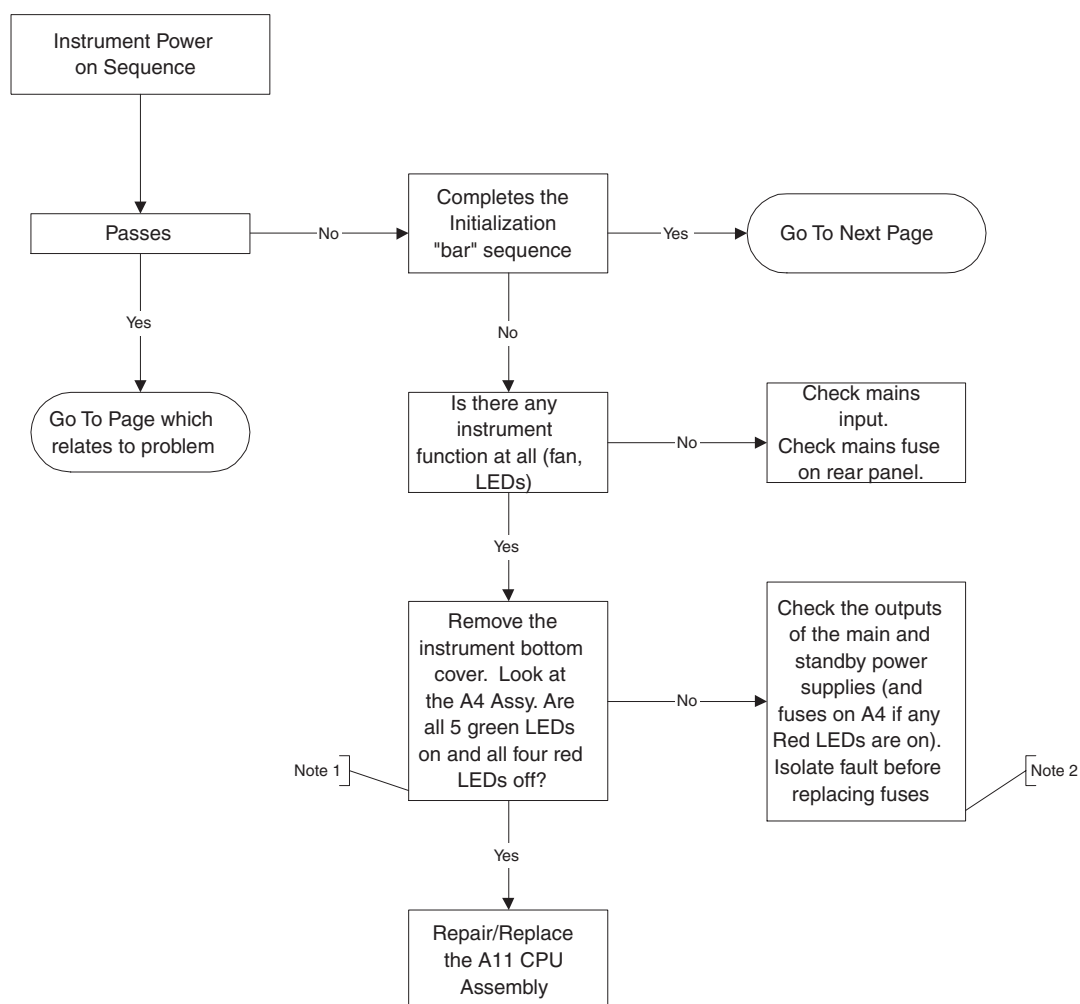


Figure 6-1: Fault Isolation Tree: Power On Sequence

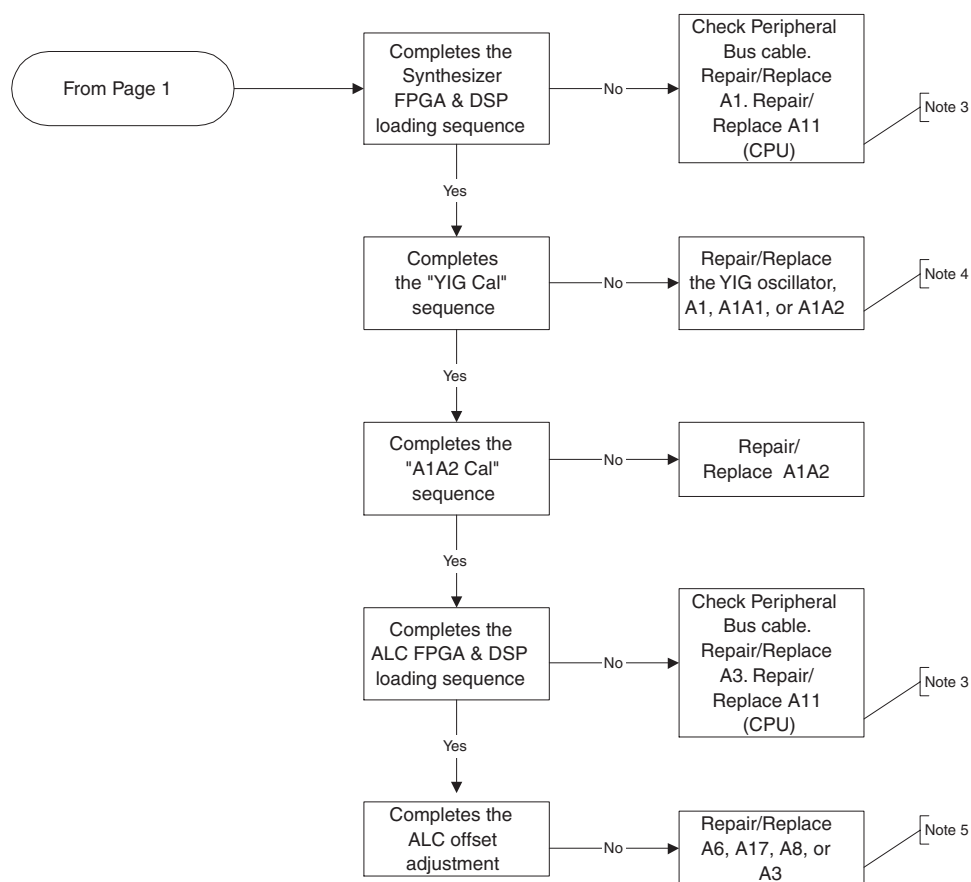


Figure 6-2: Fault Isolation Tree: Power On Sequence (Continued)

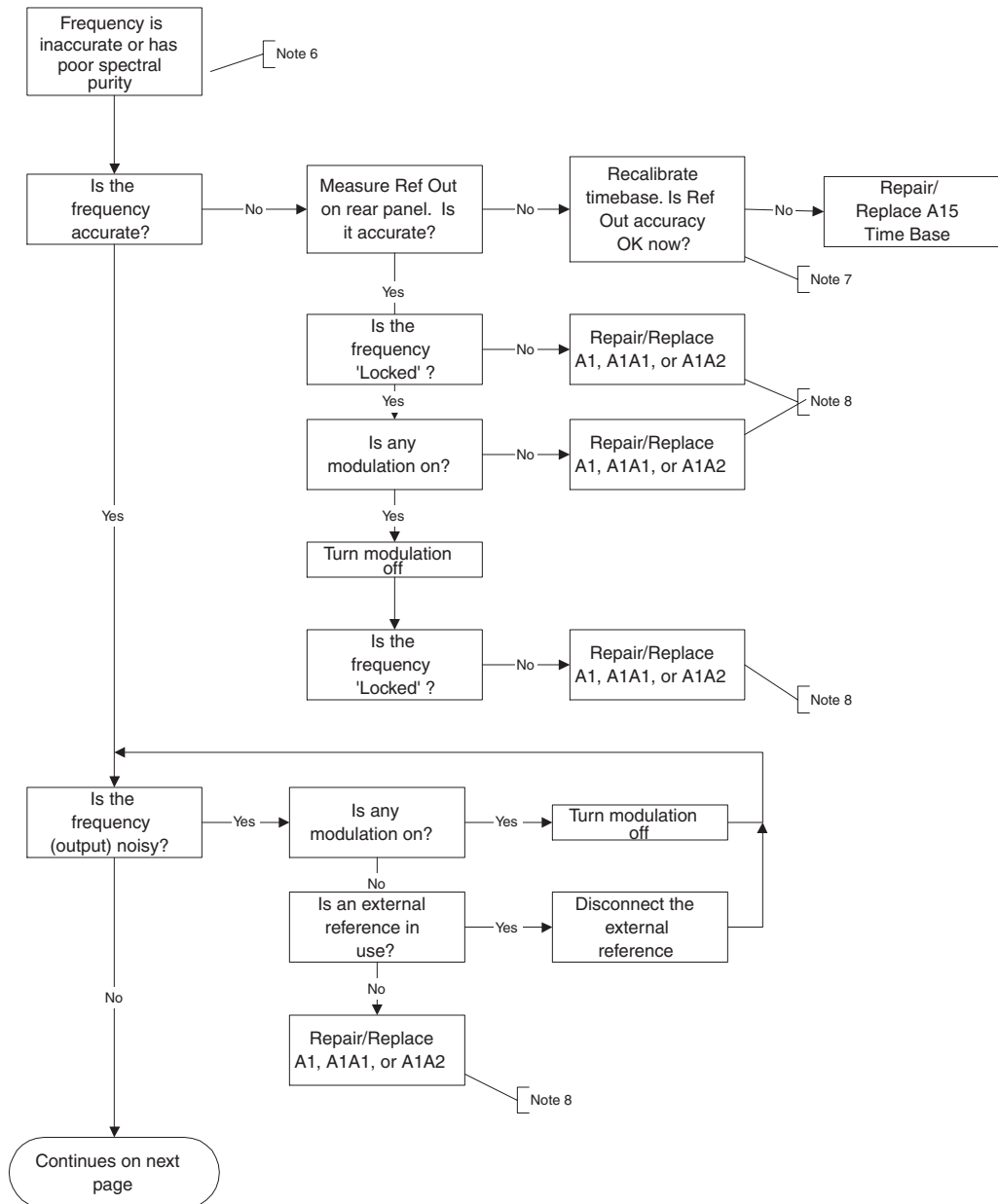


Figure 6-3: Fault Isolation Tree: CW Operation - Frequency

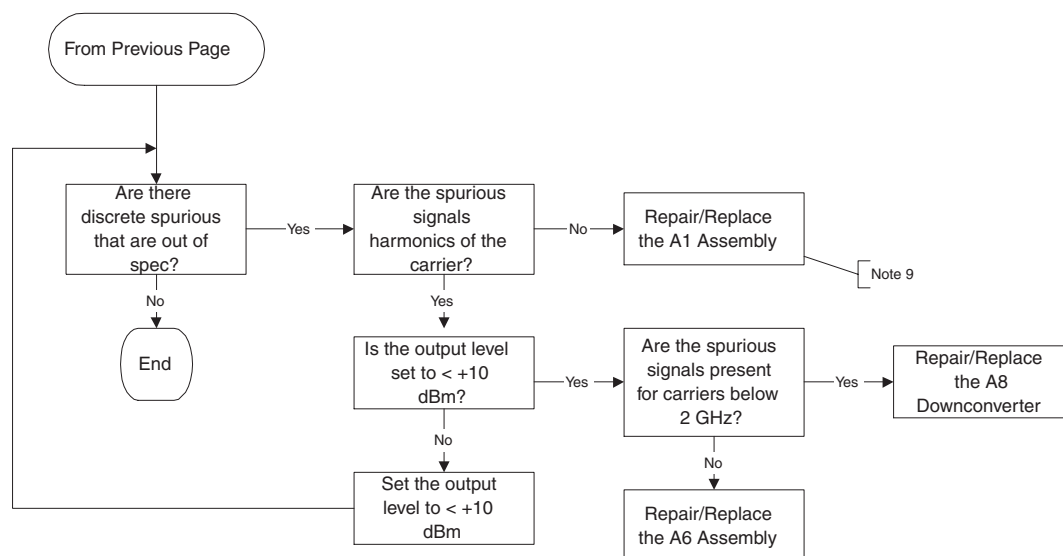


Figure 6-4: Fault Isolation Tree: CW Operation - Frequency (Continued)

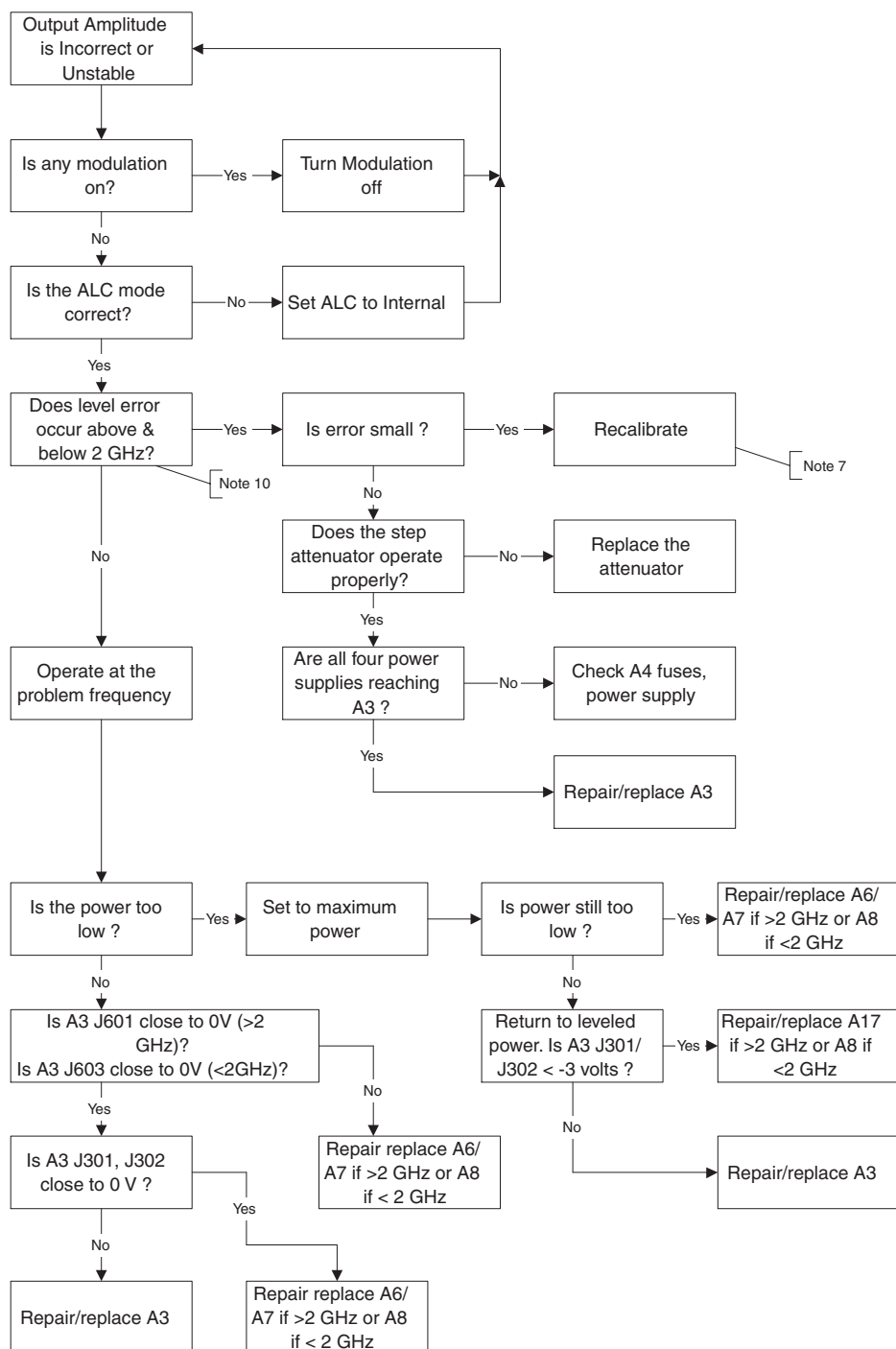


Figure 6-5: Fault Isolation Tree: CW - Level

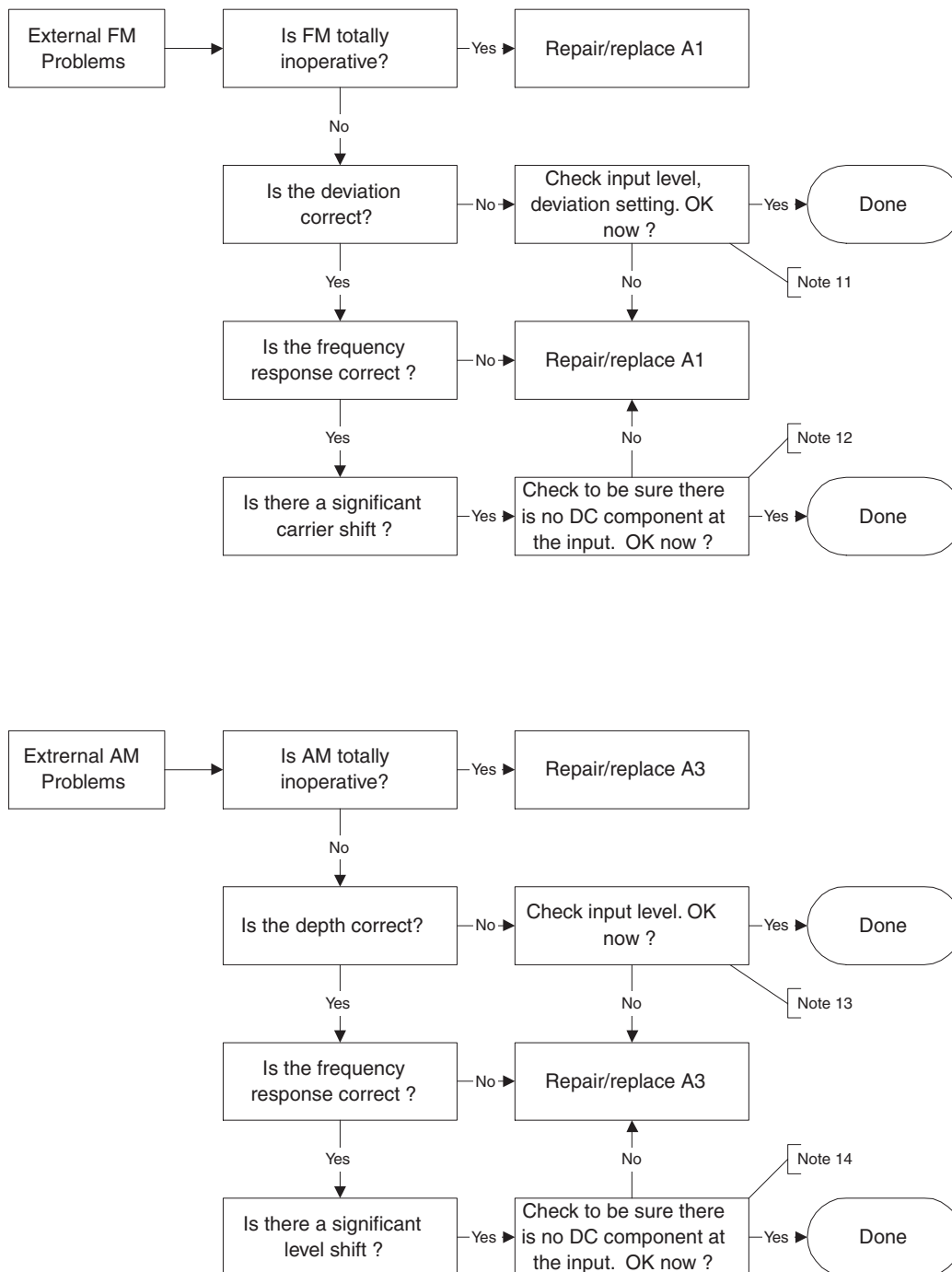


Figure 6-6: Fault Isolation Tree: Modulation Modes

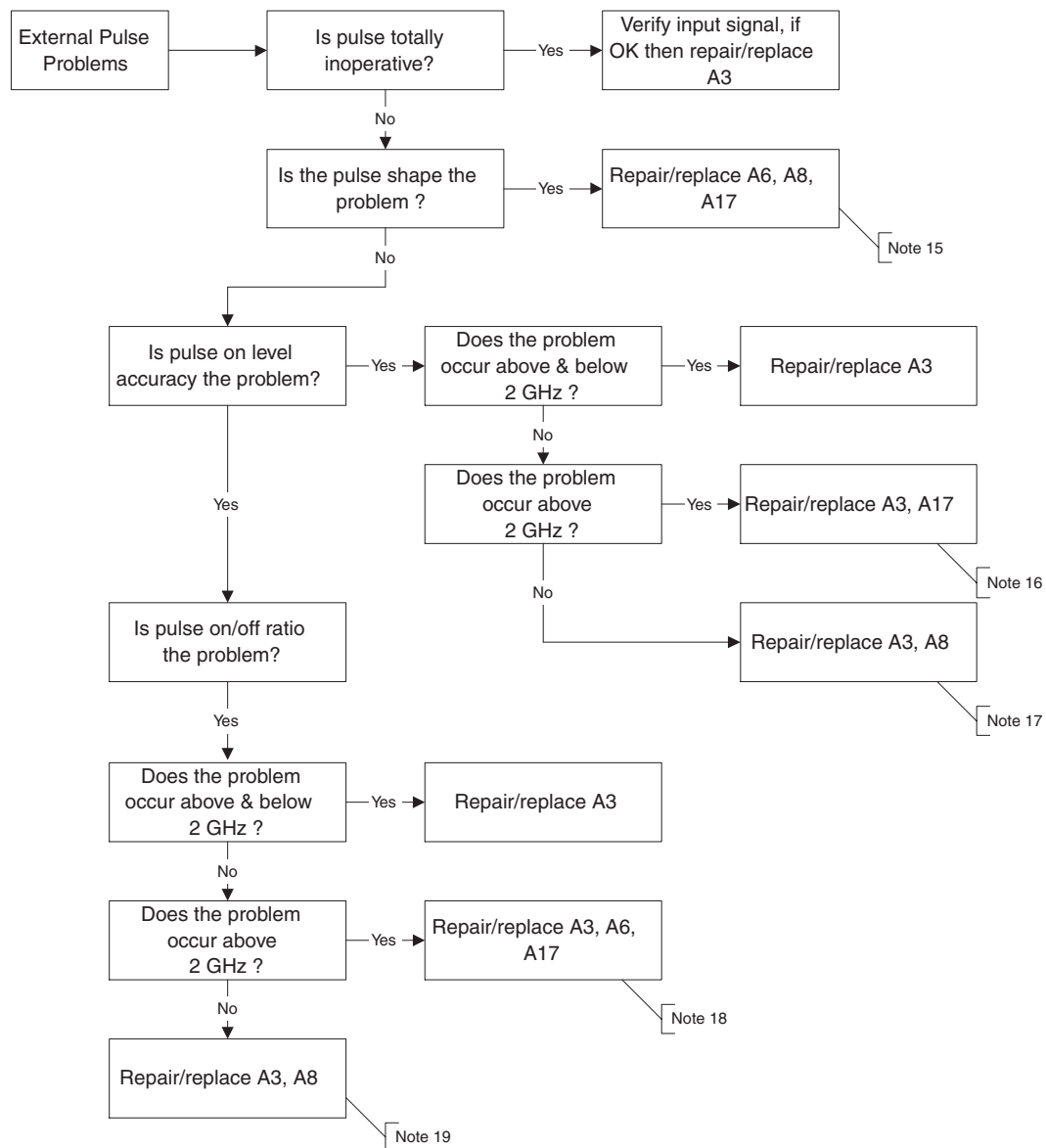


Figure 6-7: Fault Isolation Tree: Modulation Modes (Continued)

Notes:

1. The referenced LEDs are located on the edge of the A4 Distribution PC board away from the power supply assembly. Green LEDs indicate that the monitored power supply is on (they do not indicate that the supply is within tolerance). Monitors are provided for the +12 standby supply and the ± 6 and ± 12 volt main supplies. Red LEDs indicate that the corresponding power supply fuse is open. Monitors are provided for the ± 6 and ± 12 volt main supplies.
2. To isolate the power supply loads, unplug the 9 pin connectors which connect the power cables from the A4 Distribution board to the other PC assemblies. It will be necessary to remove the A1 Synthesizer assembly to access these connectors.
3. The Peripheral Bus Cable is a 60 wire ribbon cable that connects the A4, A1, A11, A3 and A16 (if installed). It is recommended that this cable be verified first before replacing any of the PC assemblies.
4. The "YIG Cal" sequence sets the YIG to 4.5 and 7.5 GHz and adjusts the tuning current to center the PLL. A failure at this point can be further isolated by removing the Instrument bottom cover then removing the coaxial cable from A1A1 J402. *This cable goes to the A6 Microwave Module. It is a .085 Semiflex about 4" long.* Connect a spectrum analyzer to J402. If a signal is present at about +10 dBm, then the YIG is working. If not, measure the voltage on the end of R724 closest to the board edge. It should be *approximately* 0.1 volts/GHz. If the voltage is outside the range of 0.4 to 0.85 volts, the oscillator may not operate and the A1 board should be serviced. A problem in A1A1 or A1A2 can also cause the YIG Cal to fail.
5. The ALC Offset calibration requires that the detectors in A6 and A8 (if installed) be functioning as well as the circuitry on A17 and A8 that amplifies the detector signals. If possible, verify the signal levels from A17 and/or A8 before replacing assemblies.
6. This problem includes frequency errors, phase noise problems, and both harmonically and non-harmonically related spurious signals. It is appropriate to determine over what range of carrier frequencies and output amplitude levels the problem exists. This will often provide additional information to help isolate the cause.
7. See the calibration and adjustment section of this manual for the procedure.
8. If available, exchange the A1A1/A1A2 assembly with a know good set and see if this fixes the problem. If so, determine which of the two is at fault. If not, replace the main A1 assembly. No re-calibration is needed if just A1A1 and/or A1A2 is replaced. FM re-calibration is needed if A1 is replaced.
9. Although the A1 assembly may be the point of entry for the spurious signals, poor connections on ground or power supply leads should be checked. The power supply itself may be producing ripple outside the specified levels. Also check if the spurious signal levels are affected by the amplitude setting. If so, the A3 ALC assembly or one of the RF modules may be at fault. Try looking at the output of A1A1 at J402 with a spectrum analyzer and see if the spur is still present.
10. A 'Yes' answer here should be used only if the level is neither at minimum nor maximum.
11. Check the input level at the FM input connector (the front and rear ones are tied together). Instrument calibration assumes that this level is 2 Vpp. Check the setting for the deviation by pressing the FM button. Note that since the instrument uses frequency multiplication and division, the maximum deviation is reduced as the frequency is reduced. If, for example, you set a deviation in narrow mode of 1 MHz at 4 GHz and then change the frequency to 1 GHz, the deviation will automatically change to 250 kHz.
12. The FM Narrow mode is DC coupled. Any DC component on the input signal will shift the carrier at the same scaling as the deviation. If, for example, the deviation is set to 1 MHz and there is 10 mV of offset, there will be 10 kHz of carrier shift.
13. Check the input level at the AM input connector (the front and rear ones are tied together). Instrument calibration assumes that this level is 2 Vpp. Check the setting for the depth by pressing the AM button.
14. The AM mode is DC coupled. Any DC component on the input signal will shift the carrier level as would the peak of an AC component.
15. If the pulse shape (rise/fall time; overshoot, etc) is a problem below 2 GHz, then replace the A8 downconverter (all pulse shape determining circuits are on this assembly). If the problem is above 2 GHz the cause could be on either the A17 board (driver) or the A6 assembly (modulator).
16. Pulse level accuracy (when the RF is on) problems which occur above 2 GHz would most likely be caused by a fault on a the A3 assembly. It is possible, however, that a defect on the A17 assembly could cause a problem since the detector buffer amplifier is located here.
17. Pulse level accuracy (when the RF is on) problems which occur below 2 GHz would most likely be caused by a fault on a the A3 assembly. It is possible, however, that a defect on the A8 assembly could cause a problem since the detector buffer amplifier is located here.
18. Pulse on/of ratio problems could be caused by the amplifiers on the A3 assembly, the driver amplifiers on A17 or by the RF module A6.
19. Pulse on/of ratio problems could be caused by the amplifiers on the A3 assembly or by the driver amplifiers and modulators on A8.

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