SCATTERING REGIMES: (Depends on ratio λ/L)

High Frequency: $\lambda \ll L$, Optics like scattering, mostly independent scattering centers, angle of incidence = angle of reflection (backscatter, surface normal points back toward radar); Signature is coherent sum (phasor addition) of scattering centers.

Coherent Sum:
$$\boldsymbol{\sigma} = \begin{vmatrix} N \\ \Sigma \\ i = 1 \end{vmatrix} \sqrt{\boldsymbol{\sigma}_i} \exp(-j2\mathbf{k} \cdot \mathbf{r}_i) \end{vmatrix}^2$$

Incoherent Sum: $\sigma = \Sigma \sigma_i$

Resonant Region: $\lambda \sim L$, Surface traveling, edge, and creeping waves become important scattering mechanisms. Must have component of E in direction of propagation. Grazing angle phenomena. Max amplitude at

$$\boldsymbol{\theta}_{\text{max}} = 49\sqrt{\boldsymbol{\lambda}} / L \text{ degrees}$$

Maximum amplitude depends on aft reflection coefficient and surface impedance, usually less than $3\lambda^2$ for PECs.

Low Frequency (Rayleigh Region): $\lambda >> L$, Induced dipole moment. Scattering proportional to (frequency)⁴:

$$\sigma \approx (4 / \pi) k^4 V^2$$

CONSTANTS:

Permittivity:

 $\boldsymbol{\varepsilon}_{0} = 8.85 \times 10^{-12}$ Farads / meter $\boldsymbol{\varepsilon}_{r} = \boldsymbol{\varepsilon} / \boldsymbol{\varepsilon}_{0} = \boldsymbol{\varepsilon}' - j\boldsymbol{\varepsilon}'', \quad \boldsymbol{\varepsilon}'' = \boldsymbol{\sigma} / (\boldsymbol{\omega}\boldsymbol{\varepsilon}_{0})$

Permeability:
$$\mu_0 = 4\pi \times 10^{-7}$$
 Henrys/meter; $\mu_r = \mu / \mu_0$

Free space wave impedance:

$$\eta = E / H = \sqrt{\mu_0 / \epsilon_0} = 120\pi = 377 \text{ ohms}$$

Velocity of Propagation: $c = (\epsilon_0 \mu_0)^{-1/2} \approx 3 \times 10^8 \text{ m/s}$
Index of Refraction: $n = \sqrt{\epsilon_r \mu_r}$

 $= 2\pi f$

Wave Vector: Points in direction of propagation, $|\mathbf{k}| = 2\pi / \lambda$

Frequency and Wavelength relationships:

$$f \boldsymbol{\lambda} = c; \quad \boldsymbol{\omega} = ck; \quad f_{\mathsf{MHz}} = (300) / \lambda_{\mathsf{meter}}$$
$$\boldsymbol{\omega} \boldsymbol{\mu}_0 = k \boldsymbol{\eta} = 240 \boldsymbol{\pi}^2 / \boldsymbol{\lambda} = 2367 / \boldsymbol{\lambda};$$
$$\boldsymbol{\omega} \boldsymbol{\varepsilon}_0 = k / \boldsymbol{\eta} = 1 / (60 \boldsymbol{\lambda})$$

MATERIAL CHARACTERIZATION:

Bulk Impedance: $Z = \eta \sqrt{\mu_r / \varepsilon_r}$

Reflection coefficient depends on polarization. For normal incidence it is

$$R = (Z - \eta) / (Z + \eta);$$
 dB = 20 log₁₀(R)

Surface impedance of material backed by ground plane, normal incidence:

General Case:
$$Z = \eta \sqrt{\mu_r / \varepsilon_r} \text{ Tanh} (jk \sqrt{\varepsilon_r \mu_r} d)$$

Thin layer: $Z = j \boldsymbol{\eta} \boldsymbol{\mu}_r k d$, independent of ε_r .

Resistive Layer, Ohms per Square: $R = 1 / (\sigma \imath) = \rho / \imath$ Impedance of thin layer, Ohms per Square:

 $Z = -j\boldsymbol{\eta} \,/ \left[k(\boldsymbol{\varepsilon}_r \,-\, 1)\boldsymbol{\tau}\right]$

Bulk Loss Characterization: $\varepsilon'' = \sigma / (\omega \varepsilon_0) = 60\lambda \sigma = 60\lambda / \rho$

MEASUREMENTS:

Radar Equation:
$$P_r = P_t G_t G_r \lambda^2 \sigma / (4\pi)^3 R^2$$

Noise Power: $P_n(dBm) \approx -114 dBm + 10 \log B_{MHz} + NF_{db}$

Ground Plane Range:
$$h_{antenna} h_{t \operatorname{arget}} = R\lambda / 4;$$

Ideal peak gain = 16 = 12dB;
Far Field distance = $2D^2 / \lambda$.

Down Range Image:
Resolution
$$\Delta r = c / (2B) = (\lambda / 2) / (\Delta f / f),$$

Extent = N Δ r

Cross Range Image: (isar) Resolution $\Delta r = \lambda / (2\Delta \theta)$

DATA TYPES:

Probability Density Function (PDF): Probability P(σ) that σ lies between σ and σ + d σ (histogram).

Cumulative Distribution Function (CDF): $CDF(\boldsymbol{\sigma}) = \int P(\boldsymbol{\sigma}) d\boldsymbol{\sigma}$

Median:
$$CDF(\boldsymbol{\sigma}_m) = 0.5 = \int_{-\infty}^{\boldsymbol{\sigma}_m} P(\boldsymbol{\sigma}) d\boldsymbol{\sigma}$$

Geometric Average:
$$\boldsymbol{\sigma}_{g} = \left[\prod_{i=1}^{N} \boldsymbol{\sigma}_{i}\right]^{1/N} = 1 / N \sum_{i=1}^{N} 10 \log_{10} \boldsymbol{\sigma}_{i}$$

Arithmetic Average: $\boldsymbol{\sigma}_{a} = 1 / N \sum_{i=1}^{N} \boldsymbol{\sigma}_{i}$; usually $\boldsymbol{\sigma}_{a} > \boldsymbol{\sigma}_{g}$

Sector Average: Average over specified angular region

Cumulative Average: Average over increasing angular sector. At each point the cumulative average is that of the defined angular sector.

Window/Slide:		Sliding wi window,		r for averaging, e.g., 5º le
Units:	Square Met	ers	<u>dBsr</u>	<u>n</u>
	1000		30	$\sigma_{dBsm} = 10 \log_{10} \sigma_{sm}$
	100		20	
	10		10	$\sigma_{sm} = 10 * *(\sigma_{dBsm} / 10)$
	1		0	
	0.1		-10	
	0.01		-20	

ANALYTICS:

Specular Reflection: $\theta_r = \theta_i$

Transmission (Snell's Law):
$$k_{inc} \sin \theta_{inc} = k_{tran} \sin \theta_{tran}$$

Geometric Optics (specular scattering):

$$\boldsymbol{\sigma}_{go} = \boldsymbol{\pi} R_1 R_2, R_1 \& R_2 \text{ radii of curvature at specular point}$$
$$\boldsymbol{E}^s = R \sqrt{\boldsymbol{\rho}_1 \boldsymbol{\rho}_2 / ((\boldsymbol{\rho}_1 + s)(\boldsymbol{\rho}_2 + s))} \quad \boldsymbol{D} \cdot \boldsymbol{E}^{inc} \exp(-jks)$$

Physical Optics (specular and end region scattering):

current:
$$\mathbf{J}_{po} = \begin{vmatrix} 2\hat{\mathbf{n}} \times \mathbf{H}^{inc} & \text{illuminted} \\ 0 & \text{shadowed} \end{vmatrix}$$

Field: $\mathbf{H}^{scat} = \int (\mathbf{J}_{po} \times \nabla g) \, dS$

Electric and Magnetic Field Integral Equations:

$$\boldsymbol{\theta} \mathbf{E}^{tot} = \mathbf{E}^{inc} + \int \left\{ (-jk\boldsymbol{\eta} \mathbf{J}_{e}g) - (\mathbf{J}_{m} \times \nabla_{s}g) + \frac{\boldsymbol{\rho}_{e}}{\boldsymbol{\varepsilon}} \nabla_{s}g \right\} dS$$
$$\boldsymbol{\theta} \mathbf{H}^{tot} = \mathbf{H}^{inc} + \int \left\{ (-j\frac{k}{\boldsymbol{\eta}}\mathbf{J}_{m}g) + (\mathbf{J}_{e} \times \nabla_{s}g) + \frac{\boldsymbol{\rho}_{m}}{\boldsymbol{\mu}} \nabla_{s}g \right\} dS$$

 $\theta = 1$ for $r \in R_i$; 1/2 for $r \in \partial R_i$; 0 otherwise

Current Continuity: $\nabla \bullet \mathbf{J} = -\mathbf{\partial} \rho / \mathbf{\partial} t = -j\boldsymbol{\omega} \boldsymbol{\rho}$

Green's Functions:

2D:

3D:
$$\begin{cases} g = \exp(-j\mathbf{k} \cdot \mathbf{R}) / 4\pi R \\ \nabla g = (1 - jkR) \mathbf{R} g / R^2 \end{cases}$$

$$\begin{cases} g = \frac{1}{4j} H_0^{(2)}(k\rho) \\ \nabla g = \frac{k}{4j} H_1^{(2)}(k\rho) \hat{\boldsymbol{\rho}} \end{cases}$$

Method of Moments: $Z_{ii} I_i = V_i$; **W** = weight; **J** = basis

$$Z_{ij} = \langle \mathbf{W}_{i}, L(\mathbf{J}_{j}) \rangle$$

$$= +jk\eta \iint [\mathbf{W}_{i} \cdot \mathbf{J}_{j} - (\nabla \cdot \mathbf{W}_{i})(\nabla \cdot \mathbf{J}_{j}) / k^{2}]g \, dS_{i} \, dS_{j}$$

$$V_{i} = \langle \mathbf{W}_{i}, \mathbf{E}^{inc} \rangle, \quad \mathbf{E}^{inc} = \mathbf{u}^{\boldsymbol{\theta} \, or \, \boldsymbol{\phi}} E_{0} \exp(-j\mathbf{k} \cdot \mathbf{R})$$

$$R_{i}^{\boldsymbol{\theta} or \boldsymbol{\phi}} = \text{row measurement vector} = \langle \mathbf{J}_{i}, \mathbf{E}^{\boldsymbol{\theta} \, or \, \boldsymbol{\phi}} \rangle$$
Unit Vectors: $\mathbf{u}^{\boldsymbol{\theta}} = [\cos(\boldsymbol{\theta})\cos(\boldsymbol{\phi}), \cos(\boldsymbol{\theta})\sin(\boldsymbol{\phi}), -\sin(\boldsymbol{\theta})]$

$$\mathbf{u}^{\boldsymbol{\phi}} = [-\sin(\boldsymbol{\phi}), \cos(\boldsymbol{\phi}), 0]$$

$$\mathbf{k} = [-\sin(\boldsymbol{\theta})\cos(\boldsymbol{\phi}), -\sin(\boldsymbol{\theta})\sin(\boldsymbol{\phi}), -\cos(\boldsymbol{\phi})]$$

HIP POCKET ESTIMATION FORMULAS: (for backscatter, $\lambda \ll L$)

Scattering Mechanisms:

Specular, end region, leading and trailing edge diffraction, surface traveling, creeping, and edge waves, multiple bounce, tip diffraction, etc.

Constant Phase Region (specular return):

$$\sigma_{specular} = 4\pi (Effective Area)^2 / \lambda^2$$

Characteristic Dimension of Constant Phase on Curved Surface: $\mathbf{L}^{effective} = \sqrt{(R\mathbf{\lambda} / 2)}$

where R = radii of curvature at specular point

Specular (Peak) Returns (polarization independent):

Planar Surfaces:

Singly Curved Surface: $\boldsymbol{\sigma} = k R L^2$

Doubly Curved Surface: $\boldsymbol{\sigma} = \boldsymbol{\pi} R_1 R_2$, R's at specular point

 $\boldsymbol{\sigma} = 4\boldsymbol{\pi} A^2 / \boldsymbol{\lambda}^2$

Approximate Beam Width: $\Delta \theta \approx 57 \lambda / L$ (rect. distribution)

Flat Plate Formulas (sides a, b, or L):

$$\boldsymbol{\sigma} = [4\boldsymbol{\pi}(ab)^2 / \boldsymbol{\lambda}^2] \cos^2(\boldsymbol{\theta})[\sin(P) / P]^2 [\sin(Q) / Q]^2$$

where $P = ka \cos(\phi) \sin(\theta)$, $Q = kb \sin(\phi) \sin(\theta)$ Envelope \perp to Edge of Length L: $\sigma = L^2 \cot^2 \theta / \pi$ Envelope Along Diagonal (45°): $\sigma = \lambda^2 \cos^2 \theta / (\pi^3 \sin^4 \theta)$

Edge Diffraction:

Leading Edge E parallel, Trailing Edge E perpendicular:

$$\sigma \approx L^2 / \pi$$

Curved Edge: $\sigma \approx R\lambda / 2\pi$

Corner Reflectors:

Dihedral: $\sigma = 8\pi (ab)^2 / \lambda^2$ Trihedral: $\sigma = 12\pi b^4 / \lambda^2$

Surface Traveling and Edge Wave (component of E in direction of propagation on surface):

Location:	$\theta \approx 49(\lambda / L)^{1/2}$
Amplitude:	Depends on aft reflection coefficient and surface impedance along propagation path, usually $\leq 3\lambda^2$

RCS of HOLES and SLOTS:

Use Babinet's principle: Interchange E & H, use complementary geometry (e.g., slot to wire, hole to disk), then use existing analytical approaches and computer codes for Rayleigh, resonant, or optical regimes.

Small holes of radius a, ka < 1:

E₁ plane of hole:
$$\sigma \approx (16 / 9\pi)a^2 (ka)^4 [2 + \sin^2 \theta]^2$$

E₁ plane of hole: $\sigma \approx (4^3 / 9\pi)a^2 (ka)^4 \cos^4 \theta$

Slots: Traveling wave for H in direction of slot

Complementary Impedance: $Z_{comp} = 377^2 / (4Z)$

Remember: RCS from arrays of holes or slots will phasor add & subtract. Peak σ when \bot to line of holes or slot

2/97

RADAR CROSS SECTION REFERENCE

Marietta Scientific, Inc.

John Shaeffer, Brett Cooper

376 Powder Springs St., Suite 240A Marietta, Georgia 30064 (770) 425-9760 www.MariettaScientific.Com

RADAR CROSS SECTION σ : A measure of power reflected by a target. Units are square meters (area). When expressed in dB, the reference is 1 square meter, dBsm or dBm². Make non-dimensional by normalizing to wavelength, σ/λ^2 .

MONOSTATIC CROSS SECTION: RCS in the backscatter direction, i.e., receiver at same location as transmitter. Usual case.

<u>BISTATIC CROSS SECTION</u>: RCS in direction other than backscatter, i.e., receiver at different location than transmitter.

<u>POLARIZATION</u>: Direction of E vector for transmit or receive. Typically vertical or horizontal.

WAVE VECTOR k: Vector direction of propagation for EM wave. Scalar magnitude inversely related to wavelength, $k = 2\pi/\lambda$.

<u>EM WAVE</u>: Propagation of electromagnetic energy. Has electric and magnetic vector components, **E** and **H**, and direction of propagation **k**. E, H, and k are mutually orthogonal. EM wave characterized by: wavelength or frequency, direction of propagation, and polarization of **E**. Wave impedance $\eta = E/H =$ $120\pi = 377$ ohms in free space.

SPECULAR POINT, FLASH POINT, REGION OF STATIONARY PHASE: Point on scattering body where angle of incidence is equal to angle of reflection. For back scatter, this is where the surface normal points back toward the radar.

<u>SCATTERING CENTER</u>: Region of body which reflects EM energy (hot spot), e.g. specular points, multiple reflection, surface wave, or diffraction locations.

<u>SURFACE WAVE</u>: Non specular scattering mechanism dominant for resonant region bodies, $L/\lambda < 10$. Types are traveling, creeping, or edge wave which occur near grazing incident angles when the incident E field has a vector component along the body in direction of propagation.

BAND	FREQUENCY	WAVELENGTH
HF	5-30 MHz	200-33 ft.
VHF	50-300 MHz	18-3 ft.
UHF	300-1000 MHz	3-1 ft.
L	1-2 GHz	1-0.5 ft.
S	2-4 GHz	6-3 in.
С	4-8 GHz	3-1.5 in.
Х	8-12.5 GHz	1.5-0.9 in.
Ku	12.5-18 GHz	0.9-0.66 in.
Ka	26.5-40 GHz	0.45-0.3 in.